Study Of Reverberation Time Series And Echo Signal Detection In Reverberation Limited Scenarios

Sowmya S.T.V, P.Chandra sekhar

Department of ECE, GITAM Institute of Technology, GITAM University, Visakhapatnam

Abstract— An innovative approach to the generation of reverberation time series and echo detection algorithms is presented The time series approach utilizes recent developments in linear spectral prediction research in which the spectra of stochastic process are modelled as rational functions and algorithms are used to efficiently compute optimal estimates of coefficients which specify the spectra. The approach taken in this paper is to detect echo signal in two steps . In the first part the reverberation time series is generated using autoregressive formulation and in the second part echo is detected using order partition prewhiten algorithm.

Keywords- Active sonar, Reverberation, Autoregressive model, Reverberation spectrum, pre-whiten

I. INTRODUCTION

S ONAR is an acronym for sound navigation and ranging .sonar is a system that uses transmitted and reflected underwater sound waves to detect and locate submerged objects or measure the distance of underwater target. Sonar Reverberation (and radar clutter) has been modeled in a variety of ways and for a diversity of applications. Expected reverberation power (intensity) level models are perhaps the most common . In these, the expected reverberation power level at the input, output, or some intermediate point in the sonar (radar) system is estimated as a function of the environmental and system parameters. The models are useful in evaluating system performance for signal processing approaches which depend primarily upon power level, such as single beam energy detectors and matched filters. The time series simulation models can be developed to generate complex (in phase and quadrature) reverberation voltage levels in time series form, as they would occur at some point in the sonar system. The time series data can be run through emulations of alternative signal processing algorithms to evaluate relative performance of the various processes.

Reverberation is caused by seabed, sea surface and the In homogeneity of the granule in the seawater. As a noise, reverberation can influence the detection performance of target echo and cause some serious problems to active sonar .

Due to the fact that reverberation and target echo are correlative and their spectrums are close, how to restrain reverberation is a problem necessary to be solved for active sonar. Inorder to restrain the reverberation signal we are using pre whiten method here. The principle of this method is that an AR model is established from reverberation and then a whiten filter is designed using the power spectrum of this model.

II. TIME SERIES MODELING

Recent developments in linear spectral prediction (UP) techniques allow stochastic processes to be modeled in a straightforward manner. Common time series models of sampled stochastic processes, which are basic to many LSP techniques, include autoregressive (AR), moving average (MA), and autoregressive moving average (ARMA) processes. These processes can be realized as the outputs of linear digital filters driven by white noise processes, where the filter transfer functions have all-pole, all-zero, and polezero realizations for AR, MA, and ARMA processes, respectively. The digital filters can be implemented as recursive infinite impulse response (IIR) filters for AR and ARMA processes, and as a transversal finite impulse response (FIR) filter for an MA process. If the stochastic process to be modelled is nonstationary: but quasi-stationary, the digital filter realization is time varying, with time-varying poles and/or zeros.

A. Autoregressive Process

In an auto regressive model of order p, the value $\overline{x_n}$ of the complex stochastic process at time n given as a linear combination of past values and a random input ξ_n , such that

$$\overline{x_n} = -\sum_{k=1}^p b_k \overline{x_{n-k}} + \sigma \xi_n$$
⁽¹⁾

Where ξ_n is a complex white noise process with zero mean and unity standard deviation. The system transfer function H(Z), between input and output is represented in terms of model parameters as an all pole function.

$$H(z) = \frac{\sigma}{1 + \sum_{k=j}^{p} b_k z^{-k}}$$
⁽²⁾

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The poles of H(Z) are the zeros of the polynomial in the denominator and the number of poles p is referred to as the model order. The discrete power density spectrum is

$$p_m = \frac{\sigma^2 \Delta t}{\left| 1 + \sum_{k=1}^p b_k e^{-j2\Pi mk/M} \right|^2}$$
(3)

Where Δt is the sampling interval and p_m is the power at radial frequency. The problem of modeling an arbitrary stochastic process {x,, n = e-, -1, 0, 1, .-} as an AR process reduces to the selection of the model parameters. The manner in which they are selected will depend on a priori information about {x,;. A standard formulation is to select the model parameters such that the linear estimate of the process {x,} at the present time n, given the past p values of the process { X n - k , k = 1: 2, --, p } , is best in a least squares sense. That is, defining the linear estimate of order p as

 $x_n^* = -\sum_{k=1}^p \mathbf{b_k} \mathbf{x_{n-k}}$ (4) the parameters are selected such that the estimation error is

minimized in a mean square sense

$$\min_{\{a_k\}} E\{\varepsilon_n^2\} = \min_{\{a_k\}} E\{(x_n + \sum_{k=1}^p b_k x_{n-k})^2\}$$
(5)

This is the digital Wiener optimal one-step prediction filtering problem, and it leads to the specification of the $\{b_k, \sigma\}$ as the solution of the normal equations

$$\rho_{in} = -\sum_{k=1}^{p} b_k \rho_{i-k,n}$$
(6a)

 $i=1,2,...,p$

$$\rho_{on} = -\sum_{k=1}^{p} b_k \rho_{kn} + \sigma^2 \tag{6b}$$

where $\rho_{i-k,n}$ is the time-varying autocorrelation function of the nonstationary process.

$$\rho_{i-k,n} \underline{\Delta} E\{x_{n-k} x_{n-i}^*\}$$
(7)

If the spectrum (which in general is time-varying) of the process is known, then the auto-correlation function can be found by inverse Fourier transformation and the parameters $\{b_k, \sigma\}$ evaluated. If the spectrum is not known, but one has the past p values of the process, as in the above Wiener filtering formulation, then the auto covariance function can be used as a local estimate of the autocorrelation function.

$$\phi_{i-k,n} \underline{\Delta} \begin{cases} \sum_{j=n-p-i}^{n-1-k} x_{j-k} x_{j-i,}^{*} \\ \sum_{j=n-p-j}^{n-1-i} i < k & i > k \end{cases}$$
(8)

The auto covariance function can then replace the autocorrelation function in the normal equations. With this replacement ,are known as the Yule-Walker equations and will be referred to in this way in this paper, regardless of whether the auto covariance or autocorrelation functions are used in them. A variety of ways to solve the Yule-Walker equations are available. We will use the Levinson-Durbin approach . Having solved for estimates of the model parameters in this way, one can evaluate the spectral estimate or the linear estimation filter transfer function &z) by using the parameter estimates in expressions (3) and (2), respectively.

The filter will produce a statistical realization of the process $\{x\}$ when driven by white noise. The spectral estimate is sometimes referred to as the maximum entropy spectral estimate.



Fig-1. Linear Spectral Prediction Approach To Modeling Stochastic Quasi-Stationary Coherent Time Series.

The Levinson-Durbin algorithm is utilized to solve the Yule-Walker equations to obtain the optimal set of non stationary poles, or more precisely, the optimal set of non stationary filter coefficients for each beam.



Fig-2. Processing Flow Of Reverberation Simulation Model.

The generation of coherent reverberation which is correlated between beams and overlapping spectra is illustrated in Fig.3 ,where Ha, Hb, .-, Hn,, represent transfer functions of the linear filters associated with beams, a, b, ...,n, respectively.

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Fig-3. Parallel Structure Of Coherent Multiple-Beam Time Series Filter

III. REVERBERATION SPECTRUM MODELING

The generation of a time series based on the existance of a spectrum was discussed. Here, an approach to generating the expected spectrum for sonar reverberation as a function of pertinent sonar system parameters and environmental conditions is presented. The approach is a numerical evaluation scheme based on a spatial grid approach of Ackerman for a general formulation of reverberation developed by Faure, Ol'shevskii and Middleton. This leads to the computation of surface, volume, and/or bottom reverberation spectra and Dower levels as functions of:

- a) transmit signal waveform and power level,
- b) spreading and absorption propagation losses,
- c) backscattering strength,
- d) transmit and receive beam patterns,
- e) sonar platform-ocean geometry, and
- f) sonar and scatter motion.

The formulation represents reverberation spectra at the input of a receiver after beam forming, but prior to signal processing operations. The reverberation is non stationary, in that the spectra vary with time (and range), both in their spectral shape and their power levels. The reverberation is quasi stationary, in that the rate of change with time is assumed to be small relative to the transmit pulse duration (or the reverberation correlation time). Although the formulation can be extended to relax some of the following , intrinsic assumptions include:

- a) primary scattering only,
- b) iso-sound-speed ocean,
- c) direct propagation path,
- d) narrow-band transmit signals,

e) back scattering is from a large number of randomly distributed weak discrete scatters,

f) radial velocity distribution of scatters is spatially uniform.

A. Faure, Olshevskii And Middleton Formulation:

The power density spectrum $P_f(f,r)$ of the reverberation

envelope at the receiver input from scatters at range r and frequency f, letting * designate the convolution operations given by

$$P_{f}(f,r) = \sigma^{2}(r)Y_{f}(f,r) * \left|S_{Tf}(f)\right|^{2} * D_{f}(f)$$

(9) Where

 $\sigma^2(r)$ = Total reverberation power from scatters at range *r*,

 $Y_f(f,r)$ = Sonar motion envelope (power density) spectrum resulting from sonar motion and stationary (non moving) scatters at range r,

$$\int_{-\infty}^{\infty} Y_f(f,r) df = 1$$
 (10)

 $|S_{Tf}(f)|$ = Transmit signal envelope (energy density) Spectrum,

$$\int_{-\infty}^{\infty} \left| S_{Tf}(f) \right|^2 df = 1$$
(11)

 $D_f(f)$ = Scatter motion spectrum resulting from random motion of the scatters. This is equal to the probability density function of Doppler frequencies of backscattered signals from a large number of scatters with random motion and received by a stationary (non moving) sonar which transmitted a pure tone signal. Since it is a probability function.

$$\int_{-\infty}^{\infty} D_f(f) df = 1$$
 (12)

The terms σ^2 , Y_f and D_f depends on whether the reverberation is from volume, surface or bottom scatters. The reverberation power levels are given by

$$\sigma_{\nu}^{2}(r) = \frac{p_{0}^{2}cTs_{\nu}10^{-2\alpha r}}{2r^{2}} \int_{\theta B 0}^{\theta S \Pi} b_{TR}(\theta,\psi)d\psi d\theta$$
(13)

$$\sigma_s^2(r) = \frac{p_0^2 c T s_s 10^{-2\alpha r}}{2r^3} \int_0^{\Pi} b_{TR}(\theta_s, \psi) \cos \theta_s d\psi \qquad (14)$$

$$\sigma_B^2(r) = \text{same as } \sigma_S^2(r), \text{ except } s_B \text{ and } \theta_B \text{ replace } s_S \text{ and } \theta_S \text{ respectively.}$$
 (15)

Where

Т

 p_0^2 = transmit source mean square pressure,

C = speed of sound in water (m/s)

= time duration of transmit signal (s),

r = range from mono static sonar to center of set of discrete scatterers (m),

$$\alpha$$
 = absorption loss,

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 $S_v, S_B, S_S =$ volume (m-3), surface (m-') bottom (m-2) backscattering strength, respectively,

 $b_{TR}(\theta, \psi)$ = transmit-receive product power beampattern.

$$\psi$$
 = azimuthal angle (rad),

 θ = elevation angle (rad),

 $\theta_{\rm s}$ $= \sin^{-1}(z/r)$ = elevation angle to surface at range r and sonar depth z (rad),

 $\theta_{\rm B}$ $=\sin^{-1}(zb-z/r) =$ elevation angle to bottom, at range r and sonar vertical distance above bottom of (zB - Z)(rad).

The transmit-receive beam pattern is further defined by $b_{TR}(\theta,\psi) = [b_T(\theta,\psi) + b_T(\theta,-\psi)] [b_R(\theta,\psi) + b_R(\theta,-\psi)]$ (16)

Where

 $b_{\tau}(\theta, \psi)$ = transmit power beam pattern $b_R(\theta, \psi)$ = receive power beam pattern

The surface backscattering strength can be represented as a function of surface grazing angle w i nd speed, and frequency (f) through models such as the Chapman-Harris model

$$S_{s} = 10 \log s_{s}$$

= 3.3\beta \log(\theta_{s}/30) - 42.4 \log\beta + 2.6
\beta = 158(\mathcal{vf}^{0.33})^{-0.58} (18)

The bottom backscattering strength can be represented as $S_B = 10 \log s_B$

$$=10\log(\sin^2\theta_B) - 27. \tag{19}$$

The sonar motion envelope spectrum for volume, surface, and bottom reverberation, for a sonar moving at constant speed v0 and constant direction are given by

$$Y_{vf}(f,r) = F \begin{cases} \frac{\theta S \prod_{\substack{j \in B \ 0}} b_{TR}(\theta,\psi) \exp(\frac{j4\Pi v_0 T}{\lambda}) d\psi d\theta}{\frac{\theta B \ 0}{\beta B \ 0}} \\ \frac{\theta S \prod_{\substack{j \in B \ 0}} b_{TR}(\theta,\psi) d\psi d\theta}{\frac{\theta B \ 0}{\beta B \ 0}} \\ \end{cases}$$

$$(20)$$

$$Y_{sf}(f,r) = F \begin{cases} \frac{\prod_{\substack{j \in B \ 0}} b_{TR}(\theta_S,\psi) \exp(\frac{j4\Pi v_0 T}{\lambda} \cos\theta \cos\psi) \cos\theta_b d\Psi d\theta}{\frac{1}{\beta b_{TR}(\theta_S,\psi) \cos\theta_S d\Psi}} \\ \frac{1}{\beta B \ 0} \\ \frac$$

 $Y_{Bf}(f,r)$ = same as $Y_{sf}(f,r)$ except θ_s replace θ_b . (22)



Fig- 4. Spatial Division Of Reverberation Field.

The power density spectrum Pf(f, r) of the reverberation envelope given by (9) is evaluated numerically dividing space into a set of cells, as illustrated in Fig. 6. The ocean is divided into spherical shells which represent the portion of the ocean that is ensonified by the signal wavefront at particular instants of time after transmission (and corresponding ranges). The spherical shells are subdivided into a grid with three types of cells corresponding to those which contribute to surface, volume, and bottom reverberation. The location of each cell is defined by the range and the azimuth and elevation angles to the center of the cell relative to the platform velocity vector.



Fig- 5. Reverberation Spectrum Model

IV. DETECTION OF ECHO SIGNAL IN REVERBERATION BACKGROUND

Reverberation is caused by seabed, sea surface and the in homogeneity of the granule in the seawater. As a noise, reverberation can influence the detection performance of target echo and cause some serious problems to active sonar. Due to the fact that reverberation and target echo are correlative and their spectrums are close, how to restrain reverberation is a problem necessary to be solved for active sonar. Inorder to restrain the reverberation signal we are using pre whiten method here.

A. Pre-whiten method

The principle of this method is that an AR model is established from reverberation and then a whiten filter is designed using the power spectrum of this model. Reverberation data is considered as Gaussian color noise. And the spectrum transformations between adjacent data segments are not obvious. The rationality of this hypothesis has been verified. The performance of this method is nicer even echo-toreverberation ratio is comparative low. On the premise of this hypothesis, a method using all-pole prewhiten filters is proposed based on AR model at first. Then ,based on this model ,order partition algorithim is brought forward in detail.

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The AR model of reverberation data is shown in equation

$$r(n) = -\sum_{i=1}^{p} a_{i} r(n-i) + w(n)$$
(23)

where w(n) is a Gaussian white noise with an average of 0, $\{a1, a2, ..., ap\}$ are estimated using the adjacent segment data. And its power spectrum is shown in equation (2).

$$s(w) = \frac{\sigma^2}{\left|1 + \sum_{i=1}^p a_i e^{-jwt}\right|}$$
(24)

When the parameters ai of this AR model have been estimated, the system function of pre-whiten filter is as follows:

$$H(z) = \frac{1}{1 + \sum_{i=1}^{p} a_i z^{-i}}$$
(25)

Output data y(n) is obtained by data x(n) passing the above system function

$$y(n) = x(n) * z^{-1}[H(z)]$$
(26)

The parameters of this AR model can be estimated through autocorrelation method, Burg method, Lattice recursive algorithm and so on.

B. Order Partition Pre-Whiten Algorithm

Order partition pre-whitens algorithm means that the sampled reverberation data is processed according to time order.

Firstly, reverberation data is partitioned into several segments. Supposing that the echo signal s(n) is included in the signal x(n) which is received by hydrophone during the observation time T. The pulse width of s(n) is T_p . Data x(n) is partitioned into several segments and the width of each segment is



Fig 6. Sketch Map Of Data Partition

Firstly, reverberation data is partitioned into several segments. Supposing that the echo signal s(n) is included in the signal x(n) which is received by hydrophone during the observation time T. The pulse width of s(n) is T_p . Data x(n) is partitioned into several segments and the width of each segment is T_D as manifested in Fig.1, where dT denotes offset between the adjacent kth and k+1th data segments. The following conditions should be satisfied when partitioning the data into several segments:

(1) The width of each data segment should be equivalent to the usable signal s(n) in order to satisfy the requirement of local stationarity.

(2) To ensure that the echo signal s(n) is fully included in one segment, the width of s(n) should be smaller than each data segment. The following inequation should be satisfied:

$$T_D > T_P \tag{27}$$

(3) To ensure that the echo signal s(n) is situated in the next adjacent data segment when s(n) is not completely included in a certain segment, following inequation should be satisfied:

$$dT \leq T_D - T_P \tag{28}$$

According to the actual situation, the width of each data segment is double of the usable signal and the data overlapping rate is $\frac{1}{2}$.

$$T_D = 2T_P \tag{29}$$

$$dT = 1/2(T_D) \tag{30}$$

Secondly, the AR model of the kth data segment is established. In the method, the system function of the prewhiten filter which is based on the kth data segment for the k+1th data segment is as follows:

$$H_{k}(z) = \frac{1}{1 + \sum_{i=1}^{pk} a_{k,i} z^{-i}}$$
(31)

Lastly, the output data $y_{k+1}(n)$ is obtained by passing data $x_{k+1}(n)$ through above system function:

$$y_{k+1}(n) = x_{k+1}(n) * z^{-1}[H_k(z)]$$

(32)

The flow chart of order partition pre-whiten algorithm is shown in below figure.



Fig 7:Flow Chart Of Order Partition Pre-Whiten Algorithm

V. SIMULATIONS AND RESULTS

The reverberation power spectrum using faure,olshevskii, and middeleton formulation is obtained and the tccording to the block diagram and the time series using autoregressive model is obtained.



background.

REFERENCES

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Fig-12. Time Series from the reverberation spectra

S. G. Chamberlain and J. C. Galli, "A Model for Numerical Simulation of Non stationary Sonar Reverberation Using Linear Spectral Prediction,"

simulation results indicate that this method is effective even in the background of low echo to reverberation ratio of input. Moreover, the order partition algorithm is the better approach for detecting the echo signal in reverberation

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IEEE journal of oceanic engineering VOL. OE-8, NO. 1, Jan. 1983, pp 21-36.

- [2]. H. Weinbeg, "Navy interim surface ship model(NISSM) 11,"Naval Underwater Systems Ctr., New London, CT. NUSC Tech. Publ. 372 and NUSC Tech. Rep. 4527, 1973.
- [3]. P. C. Etter and R. S. Plum, "A survey of underwater acoustic models and environmental acoustic data banks." Naval Anti- Submarine Warfare Syst.Proj. Office, Dept. of Navy.Washington DC, ASWR Tech. Rep.80-1 15,1980.
- [4] C. L. Ackerman and R. L. Kesser. "Reverberation spectrum model for matched filter homing systems." Pennsylvania State Univ. Applied Research Lab, Tech. Memo. File TM73-285, Dec. 4, 1973.
- [5]. P. Faure, "Theoretical model of reverberation noise," J. Acoust.Soc.Amer.,vol. 36. no. 2. pp. 259-266.Feb. 1964.
- [6]. V. V. Ol'shevskii, Characteristics of Sea Reverberation. English translation by V. M. Albers. New York: Consultants Bureau, 1967.
- [7]. A. D. Waite, Sonar for Practising Engineers, 3rd ed., John Wiley & Sons,Ltd., 2002.
- [8]. Robert J. Urick, Principles of Underwater Sound, 3rd ed., New York McGraw-Hill, 1983.
- [9]. Manuel Aineto, Stuart Lawson, "Narrowband signal detection in a reverberation-limited environment", Oceans 97, MTS/IEEE Proceedings, Nova Scotia, 1997, pp.27-32.
- [10]. Liang Hong, Li Zhishun, "An Adaptive Method to Detect Moving Targetin a Reverberation Background", Applied Acoustics, Vol.22, No.2, 2003,pp.26-29.