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RESEARCH ARTICLE

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PV And Q V Curve Analysis Of IEEE 9 Bus System

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ABSTRACT:-Voltage Stability analysis of voltage instability in electric power system is very crucial in order to maintain the equilibrium of the system.Voltage security is the ability of the system to maintain adequate and controllable voltage levels at all system load buses.The main concern is that voltage levels outside of a specifiedrange can affect the operation of the customer's loads. This paper presents the analysis of voltage instability of electric power system by using power-voltage (PV) curve and reactive power-voltage (QV) curve. **Introduction:-Voltagestability** is an important aspect of any power system design as it assures the system has sufficient power to meet the load demand. Power system **voltage** instability is related to the lack of reactive power resources in the network and the **voltage** can collapse when the power limit of a system is exceeded. Voltage stability in the power system is defined as the ability of a power system to maintain acceptable voltages at all bus in the system under normal condition and after being subjected to a disturbance. In the normal operating condition the voltage of a power system is stable, but when the fault or disturbance occurs in the system, the voltage becomes unstable this result in a progressive and uncontrollable decline in voltage. Voltage stability is sometimes also called load stability.

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I. CLASSIFICATION OF VOLTAGESTABILITY

Voltage stability may be classified into two categories. These are

1. Large-disturbance Voltage Stability

2. Small-disturbance Voltage Stability

Large-disturbance Voltage Stability – It is concerned with a system stability to control voltages following a large disturbance such as system faults, loss of load, or loss of generation. For determination of this form of stability requires the examination of the dynamic performance of the system over a period sufficient to capture of such devices as under load tap changing transformers, generator field, and current limiters. Large disturbance voltage studies can be studied by using non-linear time domain simulations which include proper modeling.

Small-Disturbances Voltage Stability – The operating state of a power system is said to have small disturbances voltage stability if the system has small disturbances, a voltage near loads does not change or remain close to the pre-disturbance values. The concept of small disturbance stability is related to steady state and be analyzed using a small-signal model of the system.

II. VOLTAGE STABILITY LIMIT

The Voltage stability limit can be defined as the limiting stage in a power system beyond which no amount of reactive power injection will raise the system voltage to its nominal state. The system voltage can only be adjusted by reactive power injections till the system voltage stability is maintained.

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Test system:-WSCC 9-bus test system (also known as P.M Anderson 9-bus) represents a simple approximation of the Western System Coordinating Council (WSCC) to an equivalent system with 9 buses and 3 generators. This particular test case also includes 3 two-winding transformers, 6 lines and 3 loads. The base kV levels are 13.8 kV, 16.5 kV, 18 kV, and 230 kV. The *single-line diagram* of the WSCC 9-bus case is shown below

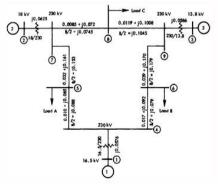


Fig 1: WSCC 9-Bus System

Here the modeling of IEEE 9 bus system is done in MATLAB /SIMULINK and investigate the behavior of Power system by Using PV and QV curves .

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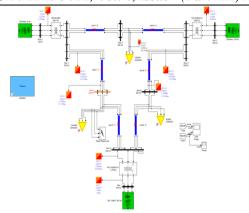


Fig 2: WSCC 9-Bus SystemMatlab Model

P-V CURVE ANALYSIS:-

P-V curve analysis is use to determine voltage stability of a radial system and also a large meshed network. For this analysis P i.e. power at a particular area is increased in steps and voltage (V) is observed at some critical load buses and then curves for those particular buses will be plotted to determine the voltage stability of a system by static analysis approach. To explain P-V curve analysis let us assume two-bus system with a single generator, single transmission line and a load, as shown in Figure.

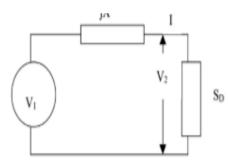


Fig 3: Two bus representation model

P-V curves are useful in deriving how much load shedding should be done to establish prefault network conditions even with the maximum increase of reactive power supply from various automatic switching of capacitors or condensers. Here, the complex load assume is with V_1 is the sending end voltage and V_2 is receiving end voltage and is load power factor.

$$P_{12} = |V_1|^2 G - |V_1| |V_2| G \cos(\theta_1 - \theta_2) + |V_1| |V_2| B \sin(\theta_1 - \theta_2)$$

 $Q_{12} = |V_1|^2 B - |V_1| |V_2| B \cos(\theta_1 - \theta_2) - |V_1| |V_2| G \sin(\theta_1 - \theta_2)$ Let G=0. Then.... $P_{12} = |V_1| |V_2| B \sin(\theta_1 - \theta_2)$

 $Q_{12} = |V_1|^2 B - |V_1| |V_2| B \cos(\theta_1 - \theta_2)$ Now we can get SD=PD+jQD=-(P21+jQ21) by • exchanging the 1 and 2 subscripts in the previous equations. • negating $P_D = -P_{21} = -|V_1||V_2|B\sin(\theta_2 - \theta_1)$ $= |V_1||V_2|B\sin(\theta_1 - \theta_2)$ $Q_D = -Q_{21} = -|V_2|^2 B + |V_1||V_2|B\cos(\theta_2 - \theta_1)$

$$= -|V_2|^2 B + |V_1||V_2| B \cos(\theta_1 - \theta_2)$$

$$P_D = |V_1||V_2| B \sin \theta_{12}$$

$$Q_D = -|V_2|^2 B + |V_1||V_2| B \cos \theta_{12}$$

$$|V_2|^2 = \frac{1 - \beta P_D \pm [1 - P_D(P_D + 2\beta)]^{1/2}}{2}$$

2

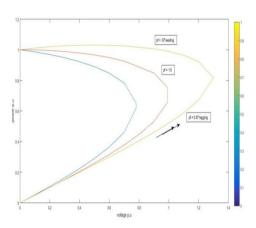
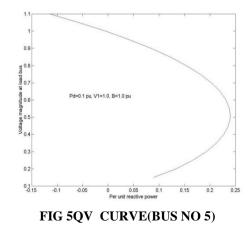


FIG 4 PV CURVE IN DIFFERENT DIFFERENTPOWER FACTOR (BUS NO 5)

QV CURVE

Q-V curve is the relationship between the reactive power support (Q) and receiving end voltage (V2) for different values of active power P [3].

$$P_{D} = |V_{1}| |V_{2}| B \sin \theta_{12}$$
$$Q_{D} = -|V_{2}|^{2} B + |V_{1}| |V_{2}| B \cos \theta_{12}$$



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METHODS OF IMPROVING VOLTAGE STABILITY The power system voltage instability can be improved using the following methods 1. Generator AVRs

- 2. Under-Load Tap Changers
- 3. Load shedding during contingencies
- 4. Reactive Power Compensation

III. CONCLUSION

Simple analytical expression for real power and reactive power at receiving end and sending end of simple two bus system has been formulated and had been used to obtain voltage V2 at load point. The same voltage expression is used to draw P-V curve Of IEEE 9 BUS system . It is observed that real power transfer increases from lagging to leading power factor. Using the Q-V curves the sensitivity of the load to the reactive power sources can be obtained. Thus basic voltage stability analysis tools i.e. P-V curve and Q-V curve are found to be effective tools to understand static voltage stability analysis.

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Appendix

								Fre	equency (Hz):	60.0	Base power (VA):	1e+08	Max iterations:	50	PQ tolerance (pu):	1e-05
	type	Bus ID	Vbase (kV)	Vref (pu)	Vangle (deg)	P (MW)	Q (Mv	Qmin (Mvar)	Qmax (Mvar)	V_LF (pu)	Vangle_LF (deg)	P_LF (MW)	Q_LF (Mvar)		Block Name	
1	ng	BUS_1	16.50	1.0400	0.00	0.00	0.00	-Inf	Inf		0.00	0.00	0.00	247.5 MVA	, 16.5 kV	
2		BUS_4	230.00	1	0.00	0.00	0.00	0.00	0.00		0.00	0.00	0.00	Load Flow	Busl	
3		BUS_5	230.00	1	0.00	125.00	50.00	-Inf	Inf		0.00	0.00	0.00	125 MW 50	MVAR/Three-Phase	e Par
4		BUS_6	230.00	1	0.00	90.00	30.00	-Inf	Inf		0.00	0.00	0.00	90 MW 30 1	WAR/Three-Phase	Para
5		BUS_7	230.00	1	0.00	0.00	0.00	0.00	0.00		0.00	0.00	0.00	Load Flow	Bus4	
6		BUS_9	230.00	1	0.00	0.00	0.00	0.00	0.00		0.00	0.00	0.00	Load Flow	Bus5	
7		BUS_2	18.00	1.0250	0.00	163.00	0.00	-Inf	Inf		0.00	0.00	0.00	192 MVA,	18 kV	
8		BUS_3	13.80	1.0250	0.00	85.00	0.00	-Inf	Inf		0.00	0.00	0.00	128 MVA,	13.8 kV	
9		BUS_8	25.00	1	0.00	100.00	35.00	-Inf	Inf		0.00	0.00	0.00	100 MW 35	MVAR/Three-Phase	e Par

PV AND QV CURVES ANALYSIS

Summary for IEEE_9bus : The load flow converged in 5 iterations

Subnetwork 1

	P(MW)	Q(Mvar)
Total generation	431.3758	1563.048
Total PQ load	315	115
Total Z shunt	0.636575	0.636565

2,	Vol. 8, Issue4 (Part -III)	April 2018, pp01-05	-					
	Total ASM	0	0					
	Total losses	115.7392	1447.411					
	$1 : BUS_1 V = 1.040 \text{ pu}/16.5 \text{kV} 0.00 \text{ deg}$; Swing bus							
	a .	P(MW)	Q(Mvar)					
	Generation	183.3758	275.2691					
	PQ Load Z shunt	0 0.216324	0 0.216316					
	BUS_4	183.1595	275.0528					
			275.0520					
	2 : BUS_2 V= 1.025 pu/18kV 11.55 deg P(MW) Q(Mvar)							
	Generation	163	712.3214					
	PQ Load	0	0					
	Z shunt	0.210128	0.210122					
	BUS_7	162.7899	712.1112					
3 : BUS_3 V= 1.025 pu/13.8kV -8.56 deg								
		P(MW)	Q(Mvar)					
	Generation PO L and	85 0	575.4573					
	PQ Load Z shunt	0.210129	0 0.210121					
	BUS_9	84.78987	575.2472					
	$4 : BUS_4 V = 0.893 \text{ pu}/$							
	1. <u>DOS_</u> 1 v= 0.095 pu/	P(MW)	Q(Mvar)					
	Generation	0	0					
	PQ Load	2.34E-09	-3.7E-10					
	Z shunt	-2.8E-06	2.77E-06					
	BUS_1	-183.157	-216.898					
	BUS_5	81.53728	144.6962					
	BUS_6	101.6202	72.20193					
	$5 : BUS_5 V = 0.743 \text{ pu}/$	P(MW)	Q(Mvar)					
	Generation	0	Q(www)					
	PQ Load	125	50					
	Z shunt	1.88E-12	-1E-12					
	BUS_4	-77.8389	-125.089					
	BUS_7	-47.1611	75.08909					
	6 : BUS_6 V= 0.799 pu/	230kV -12.95 deg						
		P(MW)	Q(Mvar)					
	Generation	0	0					
	PQ Load	90	30					
	Z shunt	2.11E-12	-3.9E-12					
	BUS_4	-98.125	-64.6108					
	BUS_9	8.124995	34.61077					
	7 : BUS_7 V= 0.599 pu/	230kV 2.01 deg						
		P(MW)	Q(Mvar)					
	Generation	0	0					
	PQ Load	1.18E-08	-1.9E-08					
	Z shunt	-1.1E-06	1.15E-06					
	BUS_2	-162.78	-394.679					
	BUS_5	52.41219	-62.4325					
	BUS_8	110.3675	457.1119					
$8 : BUS_8 V = 0.686 \text{ pu}/25 \text{kV} - 62.58 \text{ deg}$								
	Generation	P(MW) 0	Q(Mvar)					
	Generation	0	0					

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	PQ Load	100	35					
	Z shunt	1.55E-13	-1.2E-13					
	BUS_7	-57.6	-12.1851					
	BUS_9	-42.4	-22.8149					
9 : BUS_9 V= 0.698 pu/230kV -12.54 deg								
		P(MW)	Q(Mvar)					
	Generation	0	0					
	PQ Load	1.2E-09	4.56E-10					
	Z shunt	-1.7E-06	1.66E-06					
	BUS_3	-84.7834	-386.668					
	BUS_6	-6.81295	-49.0767					
	BUS_8	91.59638	435.7449					

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