

Liquid liquid extraction and separation of total rare earth (RE) metals from polymetallic manganese nodule leaching solution

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ABSTRACT:

The study on the solvent extraction for quantitative and selective separation of total rare earth metals from the polymetallic nodule leach liquor was investigated. The typical leach liquor bearing 0.094 g/L total rare earth, 0.23 g/L Mn, 0.697 g/L Cu, 0.2 g/L Fe, 0.01 g/L Co and 0.735 g/L Ni was subjected to the removal of iron content by precipitation method using $\text{Ca}(\text{OH})_2$ at pH 3.95, prior to solvent extraction of rare earth metals. Three different organo-phosphoric acid reagents (D2EHPA, PC88A, Cyanex 272) were used to ascertain their performances and selectivity towards the loading of rare earth metals in presence of other base metals. Based on the results of eq. pH effect, the performances of above three extractants followed the order as: D2EHPA > PC88A > Cyanex 272. To ensure the absence of extraction of base metals (Cu, Co, Ni), the eq. pH of the solution was optimized at the level of 2.21, though high rare earth metal extraction efficiency was observed at higher eq. pH with either of the extractants. The complete process flow diagram for substantial recovery of total rare earth was developed using D2EHPA. Extraction isotherm plot was constructed at A:O=12:1, 3-stages and $\text{pH}_e=2.21$, using 0.8 mol/L D2EHPA and the predicted condition of this study was further confirmed by 6-Cycles Counter Current Simulation (CCS) study. The stripping of total rare earth from loaded organic phase (LO) was conducted using HCl solution. McCabe-Thiele diagram study carried out at A:O=1:5 using 4 mol/L HCl showed that three theoretical stages were needed for quantitative stripping of total rare earth. The subsequent stripped solution resulted thus led to contain total rare earth of 5.6 g/L indicating a very high enrichment of total metals by solvent extraction (SX) process.

Keywords: total rare earth (RE) metals; SX; D2EHPA; HCl; deep-sea nodule

1. INTRODUCTION

Owing to the number of uses and applications in several electronics (semi/super conductors), medicine, ceramics and aerospace engineering sectors^[1,2], rare earth metals and their compounds are of huge demand in recent days. These rare earth metals are being used as novel materials with specific functions in advance technology development due to their unique spectroscopic and magnetic properties. The primary rare earth resources like Monazite, Bastnaesite^[1,3] bear considerable quantity rare elements in which the metal namely, Ce, La, Nd, Y and Pr represent as the major constituents. Nevertheless, the low grade minerals such as withered crust also contain several rare earth metals like Nd, Y, Pr etc., although the total rare earth content is very small. Similarly, low grade ore namely deep-sea nodule crust found in Pacific Ocean also claims to have a low quantity of RE (total rare earth (RE) metal ~500–1000 ppm) in addition to the existing other valuable metals i.e. nickel (1.25%–1.5%), copper (1%–1.4%), cobalt (0.2%–0.25%) and molybdenum (~0.05%)^[4,5], which can be

covered by hydrometallurgical processing route. Since total rare earth metal concentration is low, hence a suitable technology was urged to recover and enrich the total RE content from the deep-sea nodules.

Hydrometallurgical process such as leaching^[6-8] is a very common method to recover the rare earth metals from various rare earth metal bearing sources (primary/secondary) leading to the dissolution of said metal (s) into the respective lixiviant phase along with undesired other metal/impurities. Thus, the issue is the selective as well as quantitative separation of rare earth metals in presence of other metals/impurities from the subsequent leaching solution^[7]. In hydrometallurgy, the separation processes namely solvent extraction, ion exchange separation, supported liquid membrane, adsorption, and precipitation methods are very familiar while extracting the rare earth metals from numerous aqueous solutions^[9-16]. Among these, solvent extraction (SX)

method has wider range of application in hydrometallurgical separation process owing to its great potential on high selectivity, effective separation and high metal enrichment^[12]. Based on which the separation and purification of these elements (lanthanides and actinides series) by SX has gained considerable importance in recent years^[13].

The organic extractants such as di-2-ethylhexyl phosphoric acid (DEHPA), PC88A, (EHEHPA), Cyanex 272, Cyanex 301, Cyanex 302 have been extensively used for separation of rare earth metals from leaching solutions^[17-19]. The extractant like D2EHPA/TOPS 99 has a wide range of application and becomes more causative for effective and efficient extraction of rare earth metals from the various aqueous complex mixture solutions^[20]. Nevertheless, it is also found as a cost effective reagents as compared to other organophosphorous reagents and thereby, it is being regarded as one of the best suitable commercial organic extractants in solvent extraction process. In our previous studies chemical leaching of total RE was carried out using dilute H₂SO₄^[21]. At the optimum leaching condition, total RE of ~0.094 g/L along

with 0.23 g/L Mn, 0.697 g/L Cu, 0.2 g/L Fe, 0.01 g/L Co and 0.735 g/L Ni was obtained. The above leach liquor contains low concentration of total RE along with other metals such as copper, nickel, cobalt, iron and manganese in which the low content of iron is considered as the impurity. Therefore, after removal of the impurities namely iron from the leach liquor, the solvent extraction technique can be used to separate and recover total RE metals selectively. Thus, the final rare earth solution can be subjected to the production of purer rare earth compounds which is of high demand in the current stages for their numerous uses for very specific applications. As of now, the reported research works related to the recovery of rare earth metals from sea nodules is scanty. Therefore, present research investigation was aimed to describe the selective extraction of total RE metals which includes 15 rare earth metals (La, Ce, Pr, Nd, Sm, Eu, Gd, Tb, Dy, Ho, Er, Tm, Yb, Lu and Y) from the deep sea poly metallic nodule leach liquor by solvent extraction method. Initially almost all iron content was removed by

Table 1 Rare earth metal concentration in original sea nodule leach liquor (mg/L)

Name of element	La	Ce	Pr	Nd	Sm	Gd	Eu [M]
	18.6	7.08	16.25	4.26	16.64	5.665	8.5155
Name of element	Dy	Ho	Er	Tm	Yb	Lu	
	Tb [M]	6.35	1.84	3.8	0.492	670.45	61.95

1.2 Solvent extraction procedure

Equal volume of aqueous and organic phase were equilibrated for 5 min (unless otherwise specified) using separating funnel (60 mL) other than in McCabe-Thiele plots where O:A ratio was varied within the range of 1:5 to 5:1 while keeping the total volume of both phases constant. Prior to that pH of the aqueous solutions were adjusted to the desired level by addition of dilute H₂SO₄ or NaOH. After equilibration both the phases are allowed for phase disengagement followed by separation and equilibrium pH measurement. The aqueous samples were diluted to the required number of times by distilled water and the loaded organic phases were stripped with the 2 mol/L HCl (4 times) followed by diluting precipitation route followed by solvent extraction of rare earth metals by investigating with different extraction variables using D2EHPA as the extractant.

to the desired time in order to determine the concentration of RE metals as well as other base metals (Cu, Co, Ni and Mn) using ICP-AES (JOBIN-YVON JY 38 plus). All the experiments were performed at an ambient temperature (25 ± 5 °C).

The concentration of metal ion in organic phase was calculated from the difference between the metal concentration in the aqueous phase before and after extraction. The distribution coefficient (D) and percentage of extraction (% E) were calculated using Eq. (1) as described below. The chemical reaction involved on solvent extraction of RE metals with extractant can be expressed as given in Eq. (2).

$$D = \frac{V_{org}}{V_{aq}} \quad (1)$$

$$E = \frac{V_{aq}}{V_{org}} \times 100\% \quad (2)$$

1 Materials and methods

Reagents

The typical leach liquor obtained after leaching of deep sea nodule thus contains the total RE metals 0.094 g/L, Mn 0.23 g/L, Cu 0.697 g/L, Fe 0.2 g/L, Co 0.01 g/L and Ni 0.735 g/L. Table 1 shows the concentration of each of the RE metal of the original sea nodule leach liquor. The commercial acidic organic extractants namely D2EHPA, PC88A were procured from Dihalichemical limited (Japan) while CYANEX-272 was supplied by CYTECLTD (USA). These reagents were used without making any further purification. All the remaining chemicals and reagents used in this present investigation are of analytical grade (AR).



(2)

Where M=La, Ce, Pr, Nd, Sm, Eu, Gd, Tb, Dy, Ho, Er, Tm, Yb, Lu, Y, Th and R=organophosphorous extractant.

II. RESULTS AND DISCUSSION

Precipitation of iron

The actual leach liquor volume of 25 mL was taken in 100 mL beakers and pH of these solutions were adjusted to various pH values within the range 2.0–5.0 using 10% lime slurry. The samples were heated on a water bath for 1 h, cooled, filtered and analyzed. From the results as shown in Fig. 1, it can be seen that precipitation of iron was increased with increase in pH. The total iron was precipitated as $Fe(OH)_3$ and it was increased from nil at pH

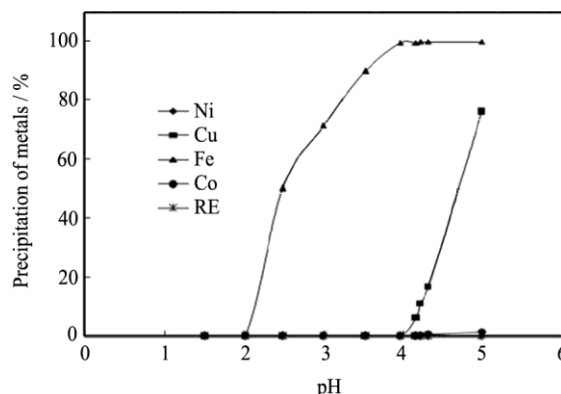


Fig. 1 Precipitation of iron at different pH

1.5) to 99.99% (at pH 4.97). Co-precipitation of other metal ions was observed during precipitation of Fe at higher pH ranges except total either of the rare earth metals. However, from the above plot, selective precipitation of Fe can be achieved at pH 3.95 without any co-precipitation of other metals. The co-precipitation of total rare earth (RE) metals or either of the rare earth metal present in the leach solution was not observed at the studied pH ranges while studying the precipitation of iron. Co-precipitation of Cu was nil up to pH 3.95 but increased beyond that pH. For example, at pH values of 4.15, 4.2, 4.3 and 4.97, the precipitation of copper (as $Cu(OH)_2$) was of 6.02%, 10.87%, 16.49% and 76.12%. The amount of copper precipitation was significantly increased with the increasing pH above 4.95, although a small quantity of Cu precipitation commenced at eq. pH 4.15 as explained above. The quantity of manganese, in the solid phase, was not observed significantly

during precipitation study up to pH 4.3 but it slowly increased up to 5.12% at pH 4.97. Manganese was co-precipitated as $Mn(OH)_2$.

It was again found that the amounts of cobalt and nickel precipitation (as $Co(OH)_2$ & $Ni(OH)_2$) was increased dramatically when the pH was increased beyond 5.0. From this study, it was evident that beyond the pH 3.95, the loss of copper was found to be high among rest of the metals and the co-precipitation of these metals follows the order as $Cu > Mn > Co > Ni$. Therefore, it was ascertained that the iron precipitation $Fe(OH)_3$ was highly selective and almost quantitative at eq. pH 3.95 and this condition was optimized for selective removal of total iron from the sea nodule leach solution. The above observations were highly supported by the literatures^[22,23] while removing the base metal impurities from the lateritic and manganese nodule sulphate leach liquor as reported by researchers.

Based on the above observations, the precipitation of Fe from the leach liquor (bulk quantity) was

carried out at an ambient temperature for 1 h. After adding the requisite amount of 10% (w/v) lime slurry in order to raise the pH of the solution up to 3.95. This Fe-free solution

(filtrate) contained 0.094 g/L total rare earth, ~1.2 mg/L (trace quantity) Fe (99.56% pptn.), 0.697 g/L Cu and 0.23 g/L Mn, 0.01 g/L Co and 0.735 g/L Ni was taken out for solvent extraction study.

Solvent extraction of total rare earth (RE) metals

Influence of organophosphorous reagents (D2EHPA, PC88A, and CYANEX 272)

Three different organic extractants such as D2EHPA, PC88A and Cyanex 272 were used for solvent extraction of RE metals. The concentration of either of the extractant was kept fixed to 0.1 mol/L and the initial pH of the solution was increased within 1.0 to 4.85. Accordingly, equilibrium pH (pH_e) of the solution was increased in the range of 0.82–2.36, 0.89–2.62 and 0.91–2.98 for the case of D2EHPA, PC88A and CYANEX-272, respectively. As shown in Fig. 2, the RE metal extraction efficiency was increased in all the three reagent cases. The RE metal extraction was increased from 2.22% to

97.22% with the increase in pH_e from 0.82 to 2.21 and thereafter, a plateau value was reached. The maximum extraction of RE metals for PC88A and Cyanex 272 were 67.4% and 57.68% at the pH_e of 2.62 and 2.98, respectively. On the other hand, there is a little co-extraction of the base metals like copper, Co, Ni and Mn was also observed at higher pH range of the solution i.e. $pH_e \geq 2.32$, $pH_e \geq 2.57$ and $pH_e \geq 2.9$ in case of D2EHPA, PC88A and CYANEX 272, respectively and these results are not shown in the above figure. Based on the results, the performance of the three reagents in terms of RE extraction, they can be ordered as D2EHPA > PC88A > CYANEX 272. The above result was further supported by the literatures^[20,24-28] and in this regard a comparison Table 2 accomplishing the performances of organophosphorous reagents while extracting the RE metal(s) from numerous aqueous solutions was provided.

From the results of the present study and the comparison with the reported literatures (as presented in Table 2) it was ensured that the usage of D2EHPA for selective and quantitative extraction as well as separation of RE metals from sulphate solution bearing the other base

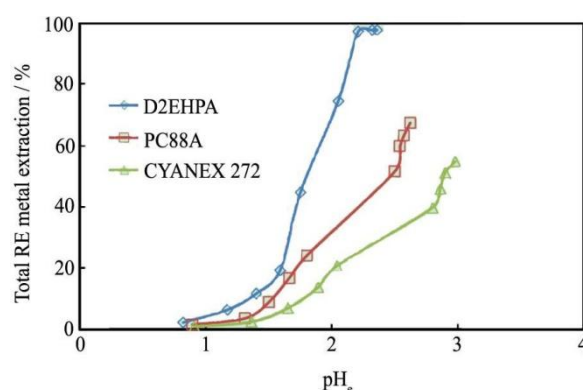


Fig. 2 Extraction profile of organophosphorous reagents at different pH_e

Table 2 Comparison on the performance of organo-phosphorous based extractants for extraction of rare earth metals

Extractant(s)	Title of articles	Remarks	Ref.
D2EHPA, PC88A, CYANEX-272	Liquid-liquid extraction and separation of total rare earth (RE) metals from the polymetallic manganese nodules leach solution	Extraction of total RE using D2EHPA is highly selective in presence of other base metals at acidic pH ranges and efficient as compared with PC88A and Cyanex 272	Parti et al. (2015) [23]
D2EHPA, PC88A	Solvent extraction of La(III) and Nd(III) from nitrate solutions with 2-ethylhexyl phosphonic acid mono-2-ethylhexyl ester	D2EHPA has higher extraction efficiency than PC88A because of high loading capacity but PC88A was found to be suitable for selective separation of La and Nd in this study	Kao et al. 2006 [24]
D2EHPA	Separation of major impurities Ce, Pr, Nd, Sm, Al, Ca, Fe, and Zn from La using bis(2-ethylhexyl) phosphoric acid (D2EHPA)-impregnated resin in hydrochloric acid medium	The use of D2EHPA impregnated with resin was promising for effective removal of RE metals and base metals	Lee et al. (2010) [25]
D2EHPA, PC88A, CYANEX-923	Distribution coefficients of La, Ce, Pr, Nd, and Sm on Cyanex 923, D2EHPA, and PC88A-impregnated resins	Large separation factors and loading of Ce, Pr, Nd, and Sm from La solution was resulted with D2EHPA as compared to PC88A, CYANEX-923	Lee et al. (2009) [26]
D2EHPA, HDEHP	Synergistic extraction of rare earths by mixtures of 2-ethylhexyl phosphoric acid mono-2-ethylhexyl ester and di-(2-ethylhexyl) phosphoric acid from sulfuric acid medium	Mixture of D2EHPA, HDEHP showed better energy for quantitative extraction of other of metals (Nd/Sm) from sulphate solution	Huang et al. (2008) [27]
HEH(EHP), D2EHPA	Process development for the recovery of high-grade lanthanum by solvent extraction	Quantitative and efficient recovery of La and Nd from chloride solution with organophosphorous reagent (s) was observed	Morais et al. (2004) [28]
TOPS99 (D2EHPA)	Solvent extraction and separation of rare earths from phosphoric acid solutions with TOPS99	Separation of rare earth metals and light rare earth metals from phosphoric acid solution was achieved using D2EHPA as the solvent reagent	Radhika et al. (2011) [29]

metals like Cu, Co, Mn and Ni at acidic pH ranges was rational while compared with other organophosphorous reagents. Therefore, D2EHPA was chosen as the best suitable extractant among the used three organo-phosphorous reagents for the RE metal extraction in the present investigation.

Influence of contact time

The effect of phase contact time for the extraction of total rare earth metals was carried out using 0.1 mol/L D2EHPA at pH 2.21 (initial pH 4.0) and contact time ranges from 0.5 to 10 min. The results of the extraction of rare earth metal with time are shown in Table 3. As expected, the total rare earth extraction showed fast rate and it was

maximized up to 97.21% just after 3 min of contact time. Thereafter, total RE extraction efficiency almost remained unaltered. However, the phase contact time of 5 min was kept fixed for further experiments.

Influence of equilibrium pH

The extraction of total rare earth metals from deep sea nodules leach liquor was carried out at the equilibrium pH range of 0.82 to 2.36 (1.0–4.85). The extraction efficiency of D2EHPA towards the extraction of total RE and other base metals at different equilibrium pH are given in Table 4. This showed that the extraction of total RE was increased from 2.22% to 97.2% with increase in

Table 3 Extraction of total RE metals at different contact time

Equilibrium time/min	0.5	1.0	2.0	3.0	4.0	5.0	10.0
Extraction of total RE/%	54.44	72.9	82.63	97.21	97.24	97.26	97.26

eq. pH of 0.82 to 2.21 and on further increase in eq. pH does not affect the RE extraction significantly. The extraction behavior of each of the rare earth metals is also shown in Fig. 3. From the results, it was ensured that the selective extraction of total RE can be obtained at eq. pH \leq 2.21 (pH 4.0). Beyond this range, the co-extraction of Mn, Cu and Ni were observed. With regards to the extraction behavior, each of these RE metals followed a similar extraction trend. From Eh-pH diagram of lanthanides [29] especially for La, Nd and Pr (since their concentration is

significantly high in the initial leach liquor as compared to other RE), they are generally highly stable at acidic pH ranges in aqueous phase at +3 oxidation state. Thereby, the extraction follows the cation exchange mechanism as described in Eq. (2) and the extraction is effective at the above studied ranges. Thus, in order to have a clean and selective separation of total RE, the pH of 2.21 was chosen as the optimum condition and it was kept fixed for subsequent studies.

Table 4 Extraction of metals at different pH levels

Initial pH	Eq. pH	Mn/%	Cu/%	Co/%	Ni/%	Total RE/%
1	0.82	0	0	0	0	2.22
1.5	1.17	0	0	0	0	6.31
2	1.4	0	0	0	0	11.64
2.5	1.59	0	0	0	0	19.26
3	1.75	0	0	0	0	44.61
3.5	2.05	0	0	0	0	74.45
4	2.21	0	0	0	0	97.21
4.5	2.32	1.73	1	0	0.14	97.63
4.82	2.36	5.63	4.3	0	0.27	97.71

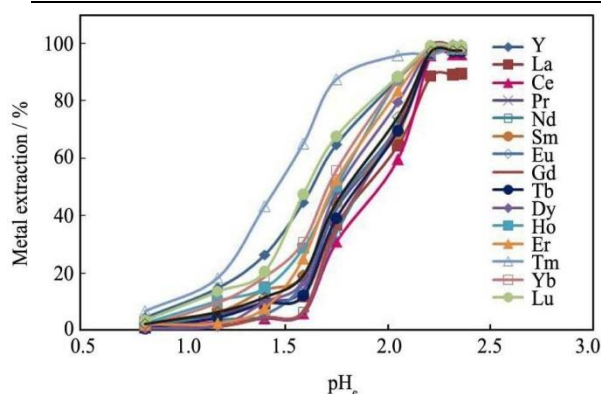


Fig. 3 Effect of eq. pH on extraction of RE metals

Influence of D2EHPA concentration

The extraction and separation of total REE from the leach liquor was carried out at varied concentration ranges (0.25 to 1.0 mol/L) of D2EHPA while keeping the value of phase ratio; A:O = 1:1, eq. pH 2.21 (pH 4.0) constant. As shown in the Fig. 4, the total REE extraction was increased from 52% to 99.6% while increasing D2EHPA concentration from 0.25 to 0.8 mol/L. Further increase in D2EHPA concentration had not affected the metal extraction efficiency to a greater extent. In addition, the co-extraction of other base metals was also not observed at the studied D2EHPA concentration ranges. Thus, from the above results 0.8 mol/L D2EHPA was found to be optimum and suitable for further Mc-Cabe Thiele plot studies, in order to achieve a high enrichment of total rare earth metals.

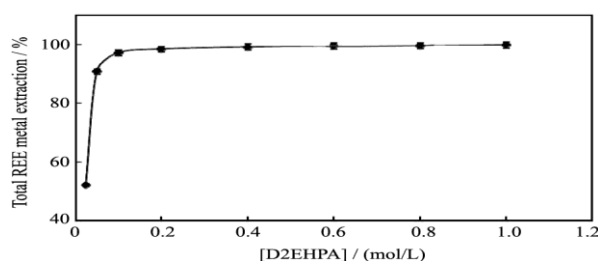
Extraction isotherm of total rare earth extraction The extraction isotherm was determined by varying

the phase ratio of A:O from 15:1 to 1:5 at equilibrium pH 2.21, using 0.8 mol/L D2EHPA. The

A:O ratio variation study was carried out to find out the theoretical number of extraction stages and the extent of enrichment of total rare earth metals in loaded organic phase during extraction. The Mc-

Cabe Thiele diagram constructed for extraction of RE metals in Fig. 5 illustrates that almost all rare earth metals of the solution were extracted to organic phase in two theoretical extraction stages at an A:O ratio of 12:1.

To confirm the above Mc-Cabe Thiele predicted condition, at two stages counter current simulation (CCS)



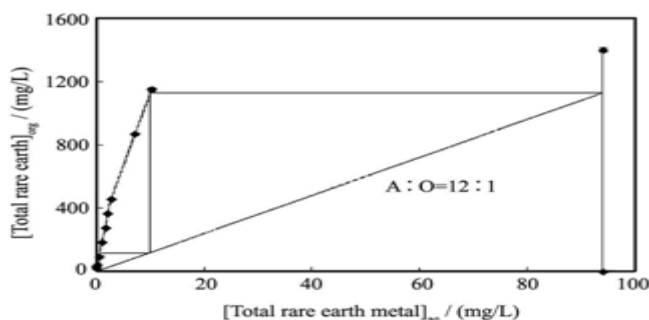


Fig.5 Mc-Cabe Thiele diagram for extraction of total RE metals

study was conducted up to 6-cycles using 0.8 mol/L D2EHPA at A: O=12:1 and equilibrium pH 2.21.

The resulted final raffinate from the above study thus results to contain ~1.0 mg/L of total rare earth ensuring 99.97% extraction of the total rare earth metal. The co-extraction of other base metal (Cu, Co, Ni and Mn) are not found and were further confirmed by loaded organic analysis. At the above mentioned condition, adequate quantity of rare earth loaded organic was generated to carry out the stripping studies.

Influence of contact time on stripping of total RE from loaded organic (LO)
As per the reported literatures^[18,20], HCl is an efficient reagent on effective stripping of rare earth metals as compared to other mineral acids. Moreover, using HCl, the rare earth metals can be easily prepared by precipitation route. Therefore, reagent HCl was used for stripping of total rare earth from loaded organic phase. The

effect of phase contact time on stripping of total rare earth from loaded organic phase was carried out using 1 mol/L HCl. As reported in the Table 5, the total RE extraction was increased from 19.23% to 74.5% with increase in the phase contact time from 0.5 to 4 min and the stripping equilibrium was attained after 4 min of phase contact time indicating a very fast back extraction. However, subsequent stripping study was carried out at 5 min of phase contact time.

Stripping of rare earth metals from loaded organic
Effect of varying concentrations of HCl in the range of 0.5–5.0 mol/L were examined for stripping of total rare earth metals from loaded organic phase. The results are shown in Fig. 6. Stripping efficiencies and phase separation of aqueous and organic phases were very good, although the quantity of HCl required for quantitative stripping was comparatively higher than the stoichiometric

Table 5 Stripping of total RE from loaded organic at different contact time

Contact time/min	0.5	1	2	3	4	5	10
Stripping of total RE/%	19.23	38.72	58.92	67.12	74.47	74.51	74.52

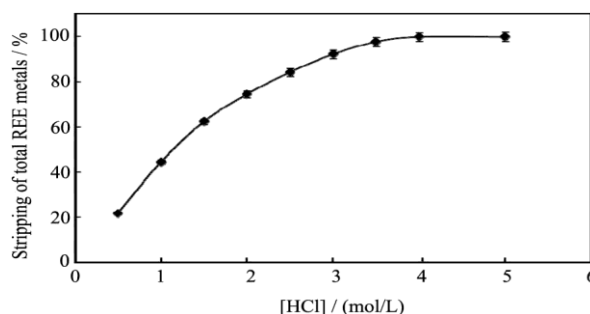


Fig.6 Effect of HCl concentration on stripping of total RE from LO

ric amount. The stripping of total RE showed an increasing trend (21.74% to 99.77%) with increasing in the HCl concentration from 0.5 to 4.0 mol/L and beyond which the stripping of total RE almost remains unaltered. Therefore, 4.0 mol/L of HCl was chosen as the optimum concentration for quantitative stripping of RE from LO and above concentration was kept fixed in subsequent studies.

Stripping isotherm studies

To find out the number of stages required for stripping at chosen phase ratio (A:O), stripping isotherm plot for total rare earth metal extraction from the loaded organic was constructed at different phase ratio in the range of A:O=1:5 to 5:1, while keeping the total volume of the phases constant. After phase separation, both phases were analyzed for metal concentration.

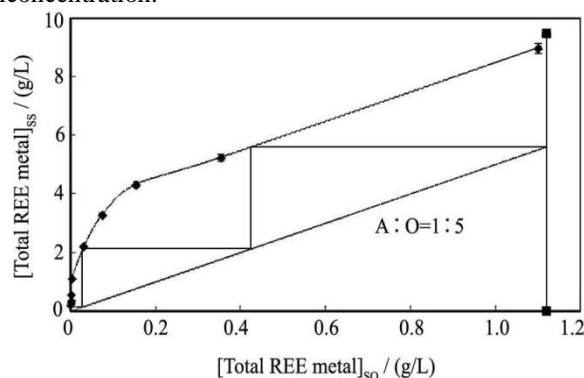


Fig.7 McCabe-Thiele diagram on stripping of total REE from loaded organic (LO)

5 times as compared to its concentration in the loaded organic. In addition, overall total RE metal enrichment was obtained as 60 folds in this process.

III. CONCLUSIONS

The actual sea nodule leach liquor bearing 0.094 g/L total rare earth metal, 0.23 g/L Mn, 0.697 g/L Cu, 0.2 g/L Fe, 0.01 g/L Co and 0.735 g/L was made iron free using $\text{Ca}(\text{OH})_2$ solution at pH 3.95 by precipitation method. Co-precipitation of other metal was not observed at the optimum iron precipitation condition. During screening of the three organophosphorous reagents (D2EHPA, PC88A and CYANEX 272) for RE extraction study, D2EHPA was found to be suitable for its higher extraction efficiency and selectivity at acidic pH range(s). The extraction efficiency followed the order as D2EHPA > PC88A > CYANEX 272. A selective and clean separation vis-à-vis a high enrichment of total rare earth from the above leaching solution was resulted in present study. Eq. pH, D2EHPA concentration, and strip solution concentration were found to be critical parameters affecting the extraction of total rare earth metal ions. Eq. pH of 2.21 (pH 4.0) was found as suitable and

As shown in the McCabe-Thiele plot (Fig. 7), more than 99% of RE metal stripping can be achieved in 3 counter-current stages at A:O ratio of 1:5. To confirm, the above prediction, a 3-stage counter-current simulation (CCS) study (up to 6 cycles) was performed. This resulted a quantitative stripping of total RE metals. From the spent organic analysis result (0.01 g/m³ of total RE) it was ensured that a quantitative stripping of total REE from the loaded organic phase. Subsequently, that led to producing the stripped solution which contains about

5.6 g/L of total REE (stripping efficiency > 99.9%), confirming the RE enrichment in the stripped solution up to

optimum condition for selective separation of rare earth

metals with ~97.21% extraction efficiency using 0.1 mol/L D2EHPA at unit phase ratio. The co-extraction of Cu, Co, Mn and Ni were not observed at the studied experimental conditions. During extraction isotherm study 0.8 mol/L D2EHPA was kept fixed and thereby, an effective and high enrichment (12 times) of rare earth metals to the loaded D2EHPA phase was achieved. During stripping isotherm 4.0 mol/L HCl was chosen as the suitable concentration and accordingly, the final stripped solution resulted thus led to bear ~5.6 g/L of total rare earth concentration. From this study, overall enrichment of total rare earth was increased to ~60 times as compared to the RE present in the original leaching solution.

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