

Evaluation of Compressive strength and Workability of normal concrete, Temperature controlled (TC) concrete and emperature controlled self-compacted (TCSC) concrete.

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ABSTRACT

The experiments conducted focuses on research to avoid shrinkage cranks and thermal expansion in concrete, the case study chosen for this experiment are underground structure having high rebar congestion. It became very critical while the mass or volume of concrete is more than natural. Generally the temperature controlled concrete for high mass or volume concrete. These type of structures are mainly foundations and under the ground only, where reinforcement area is very less and compared to concrete and concrete placing is also easy over there, but if the condition is not the same. When the situation is totally opposite of the assumption, the concrete to be done on height of more than 40 meter, and reinforcement volume is more and congestion is the condition can that concrete can't reach the bottom. Here the situation for which this paper is written. We expectingthe same situation, so our aim is to check the compressive strength and yield strength of normal concrete, Temperature controlled (TC) concrete and Temperature controlled self-compacted (TCSC) concrete.

Keywords:Temperature controlled (TC) concrete, Self-compacted Concrete (SCC), Temperature controlled self-compacted (TCSC) concrete, Strength of concrete.

I. INTRODUCTION

As the time going, the requirement of High raise Building, Heavy infrastructures likes, bridges, tunnels etc. is increasing day by day. All these big and heavy structures need strong, tough and huge foundations to complete the requirement of these structures. Generally heavy foundation in replaced by combination of two or more type of foundation like pile foundation and mat foundation or raft foundation system. But it's become tougher at those area, where SBC of foundation don't gives the minimum result for desired structure or the underground structure is not of the same nature throughout the layout. Sometime all condition match with the requirement, but the location of foundation is very much under and near to Water Level, where movement of underground structure is more than normal. So may be reason anyone from the above or it may be cost, which make the condition to use mass concrete in the foundation. As the mass concrete will give more heat of hydration, so control of temperature in concrete at the earlier stage become essential.

Temperature controlled (TC) concrete not only reduce the heat of hydration process but also decrease the shrinkage cracks and thermal expansions. Which not only increase the strength of concrete but also stability and life of structure. But when the condition came, where the temperature controlled concrete required, but the congestion of steel is too high to so that concrete cannot pass through easily to the bottom, then it's become the essential to provide the temperature controlled self-compacted concrete, so that concrete can pass through all the congested area and give the required results

Experimental details:

Material Details:The list and details of material used in the experiment is listed below,

A. Cement: The Ordinary Portland cement (OPC) of 53 grade witch is completing the standard requirement of IS269:2015. The physical properties of cement checked as per IS:4031 (Part-2) -1999 (RA 2009), IS:4031 (Part-3 to 6)-1988 (RA 2009) and results area listed in Table-1.

Sl. No.	Name of the test	Value	Requirement as per IS: 12269 - 2013
1	Consistency	29.50%	Not Specified
2	Initial Setting Time	145 min	Shal not be more than 600 Min.
3	Final Setting Time	205 min	Shal not be more than 600 Min.
4	Specific gravity	3.14	
5	Fineness of Cement	302 m ² /Kg	Shal not be less than 225 m ² /Kg
6	Soundness	0.8mm	Shal not be more than 10 mm.
7	Compressive Strength		
	a. 7 Days	47.0 Mpa	Shal not be less than 37 Mpa
	b. 28 Days	62.5 Mpa	Shal not be less than 53 Mpa
8	Density	3.12 g/cc	Not Specified

TABLE: 1(Physical - Properties of Cement)

The chemical properties of cement checked as per IS: 4032- 1985 (Reaffirmed 2009) and results are listed in Table-2

Sl. No.	Test Conducted	Results (%)	Requirement as per IS:12269-2013
1	Total Loss on Ignition (% by mas)	2.89	Not more than 4%
2	Insoluble Residue (% by mass), max	2.87	Not more than 4%
3	Ratio of % of Lime to % of silica, Alumina and Iron Oxide as per the formula.	0.89	Not greater than 1.02 and not less than 0.80
4	Ratio of % of Alumina to Iron Oxide	1.25	Not less than 0.66
5	Total Sulphur content calculated as sulphuric anhydride (% by mass)	1.50	Not more than 3.5%
6	Magnesia (MgO). (% by mass)	2.01	Not more than 6%
7	Tricalcium aluminate, (% by mass)	6.76	Not specified
8	Chloride (Cl), (% by mass)	0.017	Not more than 0.10%

TABLE: 2 (Chemical - Properties of Cement)

B. Fine aggregates: Crushed Sand has been brought from crusher yard (Uran, Maharashtra), fine aggregate passing through IS sieve, satisfying to grading Zone-II as per the IS: 383-2016 and details are listed in Table-3. The physical properties are listed in Table-4.

Sl. No.	Sieve Size	% Passing	LIMITS AS PER IS 383-2016			
	mm	Crushed Sand	ZONE I	ZONE II	ZONE III	ZONE IV
1	10.000	100.00	100	100	100	100
2	4.500	99.70	90-100	90-100	90-100	95-100
3	2.360	85.00	60-95	75-100	85-100	95-100
4	1.180	52.60	30-70	55-90	75-100	90-100
5	0.600	38.10	15-34	35-59	60-79	80-100
6	0.300	25.60	5-20	8-30	12-40	15-50
7	0.150	19.20	0-10	0-10	0-10	0-15
fineness Modulus		2.80	Note - for crushed stone sands, the permissible limit on 0.150mm sieve is increased to 20%			

TABLE: 3 (Fine Aggregates – Sieve analysis report)

SL. No.	Test Conducted	Result (Crushed Sand)
1	Specific Gravity	2.79
2	Water Absorption (%)	2.41
3	Bulk density (kg/ litre)	
a.	Loose	1.88
b.	Rodded	2.10

TABLE: 4 (Fine Aggregates – Physical Test report)

C. **Course aggregates:** Mechanically crushed angular granite stone of size 20mm and 10mm has been used, for different size of sieve used as per IS standard, which is maintained with different proportion of coarse aggregate and conforming to IS:383-2016 are listed in Table-5. The physical properties are listed in Table-6.

Sl. No.	Sieve Size	% Passing		Limits as per IS-383-2016 (single sized aggregate)	
	mm	20 mm	10 mm	20 mm	10 mm
1	40	100.00	100.00	100.00	100.00
2	20	97.00	100.00	85-100	100.00
3	12.5	32.08	100.00	-	100.00
4	10	7.80	85.75	0-20	85-100
5	4.75	0.40	1.55	0-5	0-20
6	2.36	-	1.27	-	0-5

TABLE: 5 (Course Aggregates – Sieve analysis report)

SL. No.	Test Conducted	Result		Limits as per IS-383-2016
		20 mm	10 mm	
1	Specific Gravity	2.86	2.85	-
2	Water Absorption (%)	1.33	1.44	-
3	Aggregate Impact Value (%) (12.5mm passing through 10 mm retained)	13.2	16.6	Max. 45% non-wearing surface Max. 30% wearing surface
4	Aggregate Crushing Value (%) (12.5mm passing through 10 mm retained)	13.3	16.9	Max. 30% wearing surface
5	Bulk density (kg/ litre)			
a.	Loose	1.56	1.53	-
b.	Rodded	1.69	1.65	-
6	Aggregate Abrasion Value (%)			Max. 50% non-wearing surface Max. 30% wearing surface
a.	Grading (B)	13.3	-	
b.	Grading (C)	-	15.0	
7	Flakiness Index (%)	8.1	12.0	Combined flakiness and elongation index shall not be exceed 40%
8	Elongation Index (%)	12.2	17.2	

TABLE: 6 (Course Aggregates – Physical Test report)

D. **Chemical admixtures:** Polycarboxylate ether based super-plasticizer condensate as high range water reducing admixture (HRWR) to maintain a satisfactory of workability for different mixes with constant w/b ratio throughout the experimental works. The chemical analysis report is listed in Table-7.

Sl. No.	TEST CONDUCTED	Results	Requirements (as per IS:9103-1999 (RA:2013) Table-2)	Test Method	Conformity
1	Dry Material Content, % by mass	31.27	±5% of declared Value	IS:9103:1999 (RA:2013) Clause.10.1 ANNEX E-1	-
2	Asha Content, % by mass	0.48	±5% of declared Value	IS:9103:1999 (RA:2013) Clause.10.1 ANNEX E-2	-
3	Relative Density at 25°C	1.105	±0.02% of declared Value	IS:9103:1999 (RA:2013) Clause.10.1 ANNEX E-3.1(b)	-
4	Chloride (as Cl). % by mass	0.012	±10% of declared Value	IS:6925-1973 (RA-2008) Clause:5.0	-
5	pH Value at 25°C	6.21	6.0 Minimum	IS:9103:1999 (RA:2013) Clause.10.1 ANNEX E-5	Yes

TABLE: 7 (Admixture – Chemical Analysis/ Test report)

E. Water and Ice: The type of water used for the concrete mix will affect the properties of concrete. So before starting the production of concrete, the physical as well as chemical properties to be check. And when the case arrived for temperature controlled concrete, then become essential to check all factor as per IS code 7861 (Part-1)-1975 to control the temperature of concrete mix. The quantity of ice used for lowering the

temperature is calculated as per IS code 7861 (Part-1)- 1975 recommendation and explained below:

Calculation for Ice (to find the quantity of ice to be added in concrete to produce the concrete as per targeted Temperature aggregate): As per IS: 7861 (Part-I) – 1975, the calculation of ice requirement to produce the concrete targeted temperature can be calculated.

As per equation 6.2.b (from IS: 7861 (Part-I) – 1975).

$$T = \frac{S (T_a W_a + T_c W_c)}{S (W_a + W_c) + W_w + W_i + W_{wa}} + \frac{(W_w - W_i) T_w + W_{wa} T_{wa} - 79.6 W_i}{S (W_a + W_c) + W_w + W_i + W_{wa}}$$

Where

T = Temperature of freshly mixed concrete (°C);
 T_a, T_c, T_w, T_{wa} = Temperature of aggregate, cement, added mixing water, free water on aggregate respectively (°C);
 W_a, W_c, W_w, W_{wa}, W_i = mass of aggregate, cement, added mixing water, free water on aggregate and ice respectively (Kg);
 S = Specific heat of cement and aggregate. (As per IS code it can be taken as 0.22)

Situation- 1 (For M50TC Concrete): As per above equation, the ice requirement will be calculated as per calculated data;

T* = 19 °C, T_a = 36 °C, T_c = 45 °C, T_w = 14 °C
 W_a = 1880, W_c = 513, W_w = 149, W_{wa} = 0**, W_i = to be identified

*T = Targeted Temperature (as the temperature required during placing of concrete is 21 °C)

**W_{wa} taken as zero, as no water sprinkled over aggregate.

$$19 = \frac{0.22 (36 \times 1880 + 45 \times 513) + (149 - W_i) 14 - 79.6 W_i}{0.22 (1880 + 513) + 149 + W_i}$$

$$12833.74 + 19W_i = 19968.3 + 2086 - 14W_i - 79.6W_i$$

$$19W_i + 14W_i + 79.6W_i = 22054.3 - 12833.74$$

$$112.6W_i = 9220.56$$

$$W_i = 81.888 \text{ Kg}$$

Percentage of Ice will be = (81.888/ 149) x 100 = **54.96% of Ice** against Water.

Situation- 2 (For M50SCTC Concrete): As per above equation, the ice requirement will be calculated as per calculated data;

T* = 19 °C, T_a = 36 °C, T_c = 45 °C, T_w = 14 °C
 W_a = 1663, W_c = 595, W_w = 195, W_{wa} = 0**, W_i = to be identified

*T = Targeted Temperature (as the temperature required during placing of concrete is 21 °C)

**W_{wa} taken as zero, as no water sprinkled over aggregate.

$$19 = \frac{0.22 (36 \times 1663 + 45 \times 595) + (195 - W_i) 14 - 79.6 W_i}{0.22 (1663 + 595) + 195 + W_i}$$

$$13143.44 + 19W_i = 19061.46 + 2730 - 14W_i - 79.6W_i$$

$$19W_i + 14W_i + 79.6W_i = 21791.46 - 13143.44$$

$$112.6W_i = 8648.02$$

$W_i = 76.80 \text{ Kg}$

Percentage of Ice will be = $(76.80/ 195) \times 100 = 39.39\%$ of Ice against Water.

Calculation for Ice (to reduce the water temperature from natural temperature): To reduce the existing temperature of water which is 26°C to 14°C, calculate for ice requirement the following equations has performed.

Situation- 1 (For M50TC Concrete):

To cool 1 g of water by 1°C required = 4.186 Joule to be removed

So $(149-81.88)\text{Kg}$ of water by 12°C required = $4.186 \times 12 \times 67.12 \times 1000$
 = 3371571.84 Joule to be removed

This energy is then used to melt ice.

Heat of fusion of ice = 333.55 J/g or 0.33355 kJ/g of ice

So to change 3371571.84 joule to change= $3371571.84 / 333.55$
 = 10108g or **10.11 kg of ice**

Situation- 2 (For M50SCTC Concrete):

To cool 1 g of water by 1°C required = 4.186 Joule to be removed

So $(195-76.8)\text{Kg}$ of water by 12°C required = $4.186 \times 12 \times 118.2 \times 1000$
 = 5937422.4 Joule to be removed

This energy is then used to melt ice.

Heat of fusion of ice = 333.55 J/g or 0.33355 kJ/g of ice

So to change 5937422.4 joule to change= $5937422.4 / 333.55$
 = 17800g or **17.8 kg of ice**

F. Concrete Mixture proportion and casting of specimens: The mix is designed with the guideline given in IS: 10262:2009 and with the help of ACI-211.1-91. All the details and proportion provided in Table-8. A total of 3 different concrete mixtures were proportioned based on practical requirement of materials. For temperature controlled concrete, Ice is added to water to lower the temperature from its natural

temperature level. The concrete mixtures were mixed using 50 litres capacity Pan Mixer (shown in Fig-1) and specimens were casted by using the steel mould of standard cube 150x150x150mm (3 cubes of each mix design). The fresh concrete mixtures in moulds were compacted using table vibrator and the specimens were remoulded after 24 hours after casting and water cured at $27 \pm 3^\circ\text{C}$ until the age of testing at 7 and 28 days as shown in figure 2.

Sl. No.	MATERIAL DESCRIPTION	CONCRETE MIX DETAILS			
		M50NC	M50TCC	M50TCSCC	
1	CEMENT (in Kg)	450	213	450	
2	FLY ASH	120	0	0	
3	GGBS	0	300	145	
4	C. sand	653	837	1031	
5	AGGREGATE	10mm	539	522	632
		20mm	500	521	0
6	WATER (in Litre)	165	149	175	
7	ADMIXTURE	QTY.	3.99	5.64	5.95
		PERCENTAGE	0.70%	1.10%	1%

TABLE: 8 - Mix Proportions (Value for 1 cu-m of Concrete)



Fig-1: Pan Mixer (Experimental Setup for Concrete Mixing)



Fig-2: Experimental Setup for Compressive test

Experimental Test Results and Discussion

A. Compressive Strength: The concrete compressive strength can be achieved fully by replacing the partial percentage of cement, which

not only the temperature of concrete during the process of heat of hydration but also provide the desired results. The result shown in the Table-9 to confirm the above statement.

Concrete Mix	Mix ID	7 DAYS	28 DAYS
M50 - NC	M1	41.20	59.15
	M2	43.50	63.80
	M3	42.95	60.35
M50-TCC	M4	32.05	51.50
	M5	30.90	50.65
	M6	32.35	49.75
M50-TCSCC	M7	31.95	50.90
	M8	33.30	49.45
	M9	30.90	50.05

TABLE: 9 – Compressive Strength in MPa

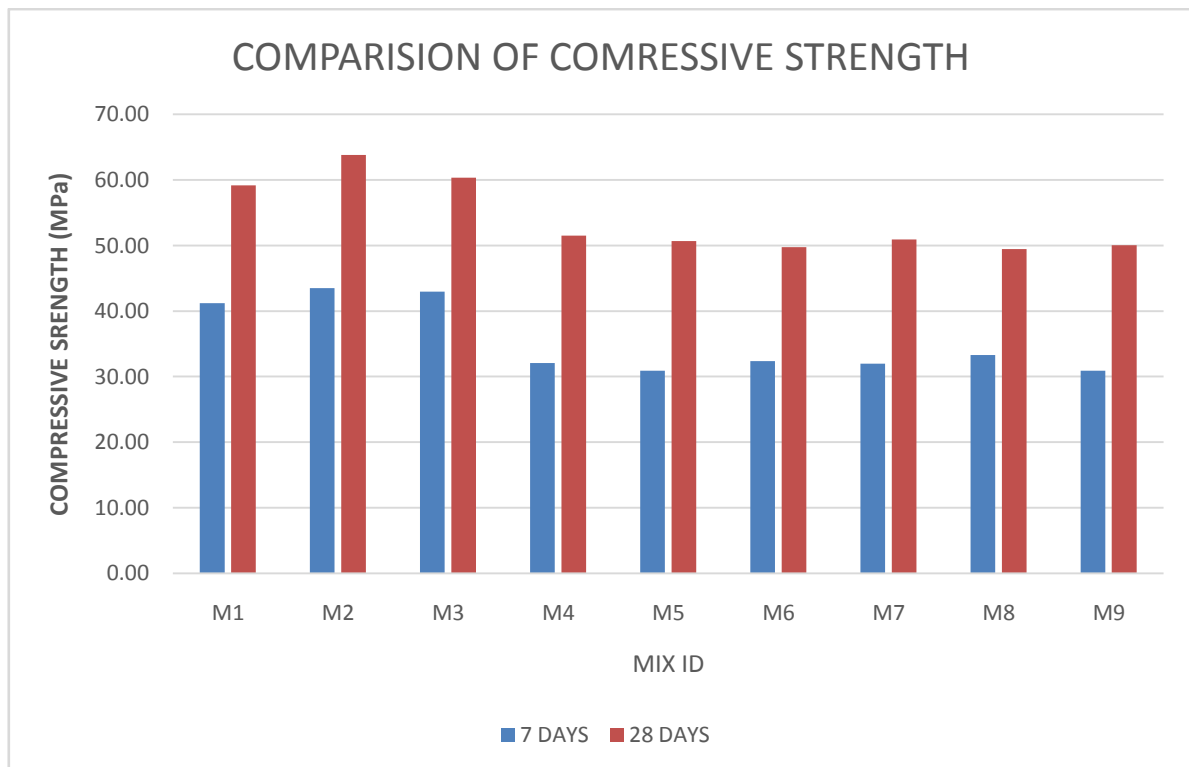


Fig-3: Comparison of Compressive Strength

B. **WORKABILITY:** The Increase in percentage of fine aggregates without increasing the percentage of admixture but by reducing the percentage of GGBS and increase the cement content will provide the great flow table which

shows the increment in the workability and give the confirmation of self-compaction. The same has been found in laboratory result and listed in the final result table-9.

Sl. No.	DESCRIPTION		NORMAL CONCRETE	TEMPERATURE CONTROLLED CONCRETE	TEMPERATURE CONTROLLED SELF COMPACTED CONCRETE
1	Grade of Concrete		M50	M50	M50
2	Flow Table		550	510	650
3	Temperature (in °c)	at the time of mixing	37	19	19
		at the time of Transportation	38	20	20
		at the time of Placing	39	21	21
4	Compressive Strength (in MPa)	7 Days	42.55	31.77	32.05
		28 Days	61.10	50.63	50.15

TABLE: 8 – Final Report Card

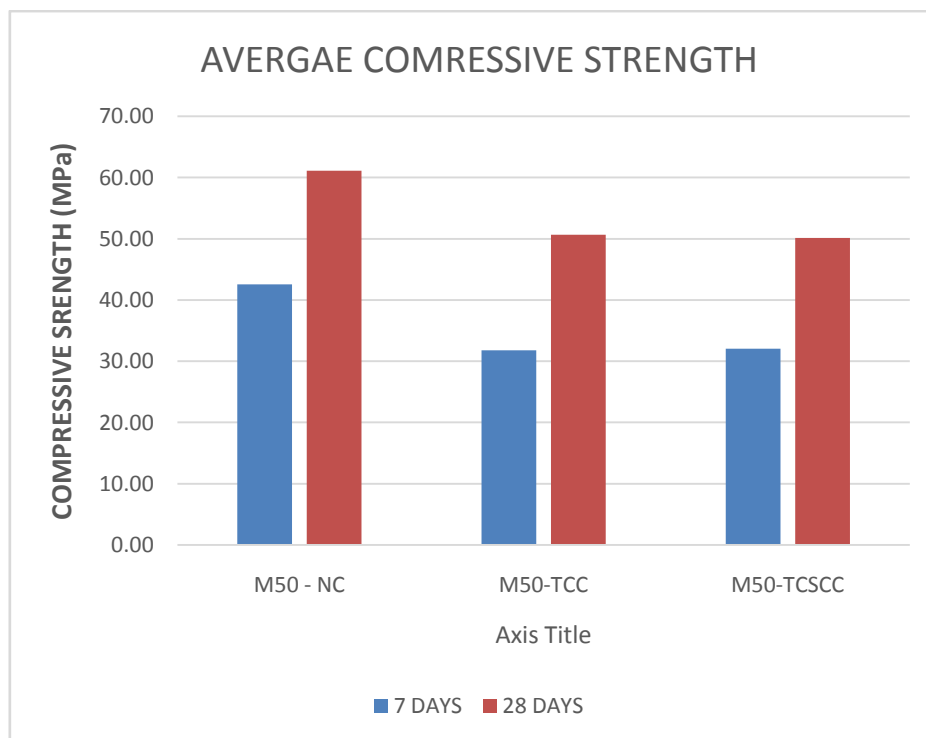


Fig-4: Comparison of Average- Compressive Strength

II. CONCLUSIONS

Based on the research study the following conclusion are drawn from the test results:-

- The compressive strength developed in TC concrete is slow. So where the early strength required, this concrete will not give desired result.
- These type of concrete cannot be used for PT structures as desired can be achieved only on 56 days compressive strength chart.
- The temperature control of concrete can be achieved by partial replacement of cement with GGBS.
- The addition of ice in water instead of adding ice in concrete, just before adding water into mix will reduce the effect on compressive strength of concrete.
- GGBS is not only reduce the requirement of cement content but also provide great help in reducing the temperature of concrete during hardening stage.
- For self-compacted temperature controlled concrete, the GGBS quantity should be less with respect to cement to achieve the desired compressive strength.

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