Non-Newtonian Visco-elastic Heat Transfer Flow Past a Stretching Sheet with Convective Boundary Condition

P H Veena, D Vinuta, V K Pravin
Dept. of Mathematics, Smt. V.G. College for Women, Gulbarga, Karnataka, India
Dept. of Mathematics, Gulbarga University, Gulbarga, Karnataka, India
Dept. of Mech. Engg., P.D.A. College of Engg., Gulbarga, Karnataka, India

ABSTRACT
In this paper two dimensional flow of a viscoelastic fluid due to stretching surface is considered. Flow analysis is carried out by using closed form solution of fourth order differential equation of motion of viscoelastic fluid. Further (Walters’ liquid B’ model) heat transfer analysis is carried out using convective surface condition. The governing equations of flow and heat transfer are non-linear partial differential equations which are unable to solve analytically hence are solved using Runge-Kutta Numerical Method with efficient shooting technique. The flow and heat transfer characteristics are studied through plots drawn. Numerical values of Wall temperature are calculated and presented in the table and compared with earlier published results which are in good agreement.

Key Words: Visco-elastic (Walters’ liquid B’) fluid, stretching sheet, convective boundary condition, heat transfer, flow analysis

I. INTRODUCTION
In reality most of the liquids are non-Newtonian in nature and are used abundantly in many engineering applications, such as plastic film manufacture, artificial fibers manufacture, aerodynamic extrusion of plastic sheets, cooling of metallic sheets in a cooling bath on process, in Geothermal reservoirs and in petroleum industries. Hence the study of viscoelastic non-Newtonian fluid flow and heat transfer phenomena is much more important as considered to the study of Newtonian fluids. Many researchers worked on the flow and heat transfer problems of viscoelastic fluids. Some of them are discussed below.

As we study the literature, Sakiadis [1] was a first researcher among all other investigators to study the phenomena considering boundary layer flow of viscous fluid over moving rigid surfaces. It is more appropriate to consider non-Newtonian behavior of all those fluids in the analysis of boundary layer flow and heat transfer characteristics as most of the fluids such as plastic films, and artificial fibers in industrial applications are strictly Newtonian. But these were restricted to flow and heat transfer in non-porous media. In recent years a great deal of interest has focused on the rheological effects of non-Newtonian flow through porous media.

Rajagopal et al [2] studied the flow of viscoelastic fluid over a stretching sheet. Siddappa and Abel [3] studied the flow analysis and heat transfer characteristics of viscoelastic fluid due to stretching plate in presence of suction and...

Nataraja et al [11] investigated the non-Similar solutions for flow and heat transfer problem considering a viscoelastic fluid over a stretching sheet. Abel et al [12] investigated the flow and Heat transfer characteristics in a viscoelastic boundary layer flow over a stretching sheet with viscous dissipation and non-uniform heat source. They obtained an analytical solution for the problem in terms of Kummer’s function. Aziz [13] has given a similarity solution for laminar thermal boundary layer over flat plate with a convective boundary condition for the viscous fluid. Makinde and Aziz [14] investigated the mixed convection on MHD flow of viscous fluid from a vertical plate embedded in a porous medium with a convective boundary condition is used to study the heat transfer analysis.

\[
\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0 ,
\]

(1) \[
\frac{\partial u}{\partial x} + v \frac{\partial v}{\partial y} = \nu \frac{\partial^2 u}{\partial y^2} - k_v \left\{ \frac{u}{\partial x} \frac{\partial^2 u}{\partial y^2} + v \frac{\partial^2 u}{\partial x^2} + \frac{\partial u}{\partial x} \frac{\partial^2 u}{\partial y^2} - \frac{u}{\partial y} \frac{\partial^2 u}{\partial x \partial y} \right\} ,
\]

(2) \[
\rho \frac{c_p}{\partial x} + v \frac{\partial T}{\partial y} = k \frac{\partial^2 T}{\partial y^2}.
\]

Here in above equations, \( \rho \) is the density, \( T \) is the temperature, \( \nu \) is the kinematic viscosity, \( k_v \) is the co-efficient of elasticity, \( k \) is coefficient of thermal conductivity, \( c_p \) is specific heat at constant pressure, The other quantities have their usual meaning. It is to be emphasized here that Eq. (2) is one order higher than the Navier-Stokes equation and this would require an additional boundary condition. Since we are considering a semi-infinite region such a boundary condition may be assumed in the form of an asymptotic condition at infinity. This is reflected in the following boundary conditions:


On observing above there are studies of heat transfer analysis of visous fluids with convective heating conditions, but there are no studies in heat transfer analysis of viscoelastic fluids with convective heating condition as it has more practical application in the field of engineering and industries. Hence in the present paper the investigation of flow and heat transfer analysis of viscoelastic fluid with convective heating boundary condition is studied.

II. MATHEMATICAL FORMULATION

Here it is considered the two-dimensional laminar boundary layer flow of an incompressible, visco-elastic fluid (Walters’ liquid B’ model) due to a stretching sheet as it has created due to two equal and opposite forces applied along the x-axis, so that the sheet is stretched, keeping the origin fixed. Under the boundary layer approximations and the assumptions that the contribution due to the normal stress is of the same order of magnitude as the shear stress - the basic boundary layer equations governing the flow of Walters’ Liquid B’, heat transfer in presence of non-uniform heat generation can be written as:

\[
\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0 ,
\]

(1) \[
\frac{\partial u}{\partial x} + v \frac{\partial v}{\partial y} = \nu \frac{\partial^2 u}{\partial y^2} - k_v \left\{ \frac{u}{\partial x} \frac{\partial^2 u}{\partial y^2} + v \frac{\partial^2 u}{\partial x^2} + \frac{\partial u}{\partial x} \frac{\partial^2 u}{\partial y^2} - \frac{u}{\partial y} \frac{\partial^2 u}{\partial x \partial y} \right\} ,
\]

(2) \[
\rho \frac{c_p}{\partial x} + v \frac{\partial T}{\partial y} = k \frac{\partial^2 T}{\partial y^2}.
\]

(3)
\[ u = b x, \quad v = 0, \]
\[ -k \frac{\partial T}{\partial y} = h \left( T - T_y \right) \quad \text{at} \quad y = 0, \]
\[ u \rightarrow 0, \quad \frac{\partial u}{\partial y} \rightarrow 0, \quad T \rightarrow T_w \quad \text{as} \quad y \rightarrow \infty \]

Here \( u \) and \( v \) are the velocity components along \( x \) - and \( y \)-directions respectively, where \( T_w \) is the temperature of the fluid far away from the sheet (temperature of ambient cold fluid) \( T \) is the uniform temperature on the top surface of the plate. Hence we have \( T_r > T > T_w \).

### III. FLOW ANALYSIS

Now introducing the similarity transformations in the form,
\[ u = b x f_\eta (\eta), \quad v = -\sqrt{b \nu} f (\eta) \quad (5) \]
where \( \eta = \sqrt{b \nu} y \) is dimensionless normal distance

Eq.(1) is identically satisfied with these change of variables and Eq.(2) is transformed to:
\[ f_\eta^2 - f f_\eta \eta = f_\eta \eta \eta - k_1 \{ 2 f_\eta - f f_\eta \eta \eta - f_\eta^2 \} \quad (6) \]
where
\[ k_1 = \frac{k_b b}{b} \quad (7) \]
The subscript \( \eta \) denotes the differentiation with respect to \( \eta \), \( k_1 \) is the non-dimensional visco-elastic parameter. The governing boundary conditions on velocity Eq.(4) take the following form as:
\[ f_\eta = 0, \quad f_\eta \eta = 1 \quad \text{at} \quad \eta = 0, \quad (8) \]
\[ f_\eta \rightarrow 0, \quad f_\eta \eta \rightarrow 0 \quad \text{as} \quad \eta \rightarrow \infty \]

The solution of Eq.(6) corresponding to the boundary conditions (8) is obtained as
\[ f (\eta) = \frac{1 - e^{-a \eta}}{\alpha} \quad (9) \]
where
\[ \alpha = \sqrt{1 - k_1} \quad (10) \]

The velocity components \( u \) & \( v \) become
\[ u = b x e^{-a \eta}, \quad v = -\sqrt{b \nu} \left( 1 - e^{-a \eta} \right) \quad (11) \]
where \( b > 0 \) and \( \alpha \) is given by Eq.(10).

### IV. SKIN FRICTION

The local skin friction coefficient or frictional drag coefficient is given by
\[ C_f = \frac{\tau_w}{\mu b x \sqrt{b \nu}} = \alpha, \quad (12) \]
where \( \tau_w = -\mu \left( \frac{\partial u}{\partial y} \right)_{\eta=0} = \mu b x \alpha \sqrt{b \nu} \), is the wall shearing stress on the surface of the stretching sheet, \( \mu \) is the dynamic viscosity of fluid and \( \alpha \) is given by Eq.(12).

### V. HEAT TRANSFER ANALYSIS

In this section the convective boundary condition with constant surface temperature for the heating process is considered. To solve heat equation (3) Defining the non-dimensional temperature \( \theta (\eta) \) as:
\[ \theta (\eta) = \frac{T - T_w}{T_r - T_w} \quad (13) \]
where \( T_r \) the temperature of the sheet.

Using Eqn. (13), Eqs. (3) and (4) can be converted to
\[ \theta (\eta) = B \left( 1 - \theta (\eta) \right) \quad \text{at} \quad \eta = 0, \quad (14) \]
\[ \theta (\eta) \rightarrow 0 \quad \text{as} \quad \eta \rightarrow \infty \quad (15) \]
where

\[ Pr = \frac{\mu C_p}{k} \]

is the Prandtl number.

\[ B_i = \frac{h}{k} \sqrt{\frac{\nu}{a}} \]

is the thermal Biot number

Here Biot number \( B_i \) is the dimensionless parameter and it plays the fundamental role in conduction problems that involves surface convection effects. Biot number parameter provides the measure of temperature drop in the solid relative to the temperature difference between the surface and fluid.

For \( B_i << 1 \) shows the resistance to conduction within the solid is much less than the resistance to the convection across the fluid boundary layer, hence assumption of uniform temperature is reasonable. Whereas \( B_i >> 1 \) says the temperature difference across the solid is much larger than that between surface and fluid.

VI. NUMERICAL SOLUTION

In this section we are explaining about the method of Numerical Solution used to solve the boundary value problems of considered study. The Governing equations of motion and heat transfer are highly non-linear so it is very difficult to solve, hence the partial differential equations are converted into ordinary differential equations by means of similarity transformation. The exponential exact solution of momentum equation is obtained and is used to find the solution of energy equation (14) with respect to the boundary conditions (15). The Boundary value problem considered is converted into initial value problem then by using Newton-Rapson method, the missing condition is found and then using Runge-Kutta integration scheme the solution of temperature boundary value problem is obtained. The step size is chosen as 0.001 and the accuracy of result is maintained upto 10-6.

VII. RESULTS AND DISCUSSION

After obtaining the solution of boundary value problem, various plots of flow, velocity and temperature are plotted to analyze the effect of various governing parameters.

Fig. 1. is the representation of physical sketch of considered problem. It shows how the stretching sheet problem is constructed.

Fig. 2. Is plotted for the flow profiles as well as the velocity profiles for different values of viscoelastic parameter \( k_1 \). Which show that, both the profiles decrease with increase in the parametric values of viscoelastic parameter which happens throughout the boundary layer which is obvious.

Fig. 3. is Plotted for the temperature profile which shows the effect of viscoelastic parameter. On observing the plot one can see that the temperature is increasing with increase in the parametric value of viscoelastic parameter. This is due to the fact that an increase of viscoelastic normal stress give rise to thickening of the thermal boundary layer.

Fig. 4 shows that, the temperature profile decreases with an increase in the parametric value of Prandtl number, which shows that the viscoelastic boundary layer is thicker than the thermal boundary layer.

Fig. 5 shows the effect of Biot number parameter on the temperature profile. On observing the graph it depicts the fact that temperature is increases with increase in the parametric value of Biot number as the stronger convection results in higher surface temperatures, which causes the thermal effect to penetrate strongly deeper into the fluid.

VIII. CONCLUSIONS

- Analytical Solutions for flow and numerical solution of convective heat transfer problem are obtained.
- The effects viscoelastic parameter is to decrease the flow and velocity, which was quite opposite on temperature.
- The thermal boundary layer thickness decreases with increasing Prandtl number in convective heat transfer phenomenon
- When viscoelastic parameter \( k_1 \) tends to zero, results are reduced to the Newtonian case.

REFERENCES


Fig. 1. Schematic diagram of linear stretching sheet
Fig. 2. Flow and Velocity profile for different values of viscoelastic parameter

Fig. 3. Temperature profiles for different values of visco-elastic parameter
Fig. 4. Temperature profiles for different values of Prandtl number

Fig. 5. Temperature profiles for different values of Biot number $B_i$,