

Preparation of ZrB_2 -SiC based ceramics using $MoSi_2$ as sintering aids and explanation using electronic theory of sintering – an elementary literature review

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ABSTRACT

ZrB_2 (zirconium diboride)-based ceramics reinforced by 15vol.% whiskers with high density were successfully prepared using $MoSi_2$ as sintering aids. The effects of sintering condition and $MoSi_2$ content on densification behavior, phase composition, and mechanical properties of ZrB_2 composites were studied. Nearly, fully dense materials (relative density >99%) were obtained by hot-pressing (HP) at 1700°C–1800°C in flow argon atmosphere. The grain size of ZrB_2 phase in the samples sintered by HP at 1700°C–1800°C were very fine, with mean size below 5 μm . Mechanical properties (such as flexural strength, fracture toughness, and Vickers hardness) of the sintered samples were measured. The sample with 15vol.% $MoSi_2$ addition sintered by HP at 1750°C displayed the best mechanical properties.

Keywords: zirconium diboride (ZrB_2) $MoSi_2$ sintering aids mechanical properties, Spark plasma sintering(SPS)

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I. INTRODUCTION

Zirconium diboride (ZrB_2) ceramics have been widely studied due to their combination of physical properties, such as high melting temperature (3245°C), high strength, high electrical and thermal conductivity, chemical inertness against molten metals of nonbasic slags, and superthermal shock resistance [1,2]. These properties make them currently considered as ultra-high temperature ceramics (UHTCs). However, there are three main barriers limiting the application development of ZrB_2 -based ceramics: relatively poor mechanical properties including low strength and fracture toughness, poor intrinsic sinterability because of the strong covalent bonds between Zr and B, and the poor oxidation resistance at high temperature. A lot of studies have been done in order to address the barriers limiting the application development of ZrB_2 -based ceramics. To improve the strength and fracture toughness of ZrB_2 ceramics, particles [3], whiskers [4,5], or carbon fibers [6] were used as reinforcements. However, a large amount of reinforcements will inhibit the sintering densification of ZrB_2 ceramics, which affects the mechanical properties of the ceramics. To improve the sintering densification of ZrB_2 , very high sintering temperatures (2100°C–2300°C), pressure-assisted sintering procedures, and sintering additives are usually adopted. So far, a lot of metals (e.g., Cr and Fe) and ceramic powders (e.g.,

Si_3N_4 , AlN, WC, and $MoSi_2$) were used to promote the sinterability of ZrB_2 [7–11]. $MoSi_2$ was found to be an effective additive to improve both sinterability and oxidation resistance of ZrB_2 ceramics [12–14]. In this study, $MoSi_2$ was selected as sintering aids, and SiC whisker was selected as toughness phase. The aim of this work is to study preparation and properties of the composites in the system ZrB_2 -15vol.% SiC whisker-(10vol.%–20vol.%) $MoSi_2$. The densification behavior, phase composition, mechanical properties, and micro-structure of sintered materials were investigated.

Motivation

Transition metal diborides, especially zirconium and hafnium diboride are potential ceramic material for ultra high temperature applications above 1800°C. These borides are characterized by high melting point, formation of high melting point oxides, good oxidation resistance and excellent thermo-mechanical properties. In this present exploration, zirconium diboride (ZrB_2) has been selected for its moderate density (6.09 gm/cc) and better oxidation resistance compared to high density hafnium diboride (11.2 gm/cc). SiC and $MoSi_2$ were added to improve the thermal shock resistance and sinterability of the ultra high temperature ceramics (UHTCs).

Experiment

Commercial powders were used to prepare the ceramics. ZrB₂, particle size: 10-15 μ m, purity: 99.5%, particle size: 2 μ m, purity: 99.9 %; MoSi₂, particle size: 2 μ m, purity: 99.9 %. The powder mixtures mixed with a certain volume proportion (ZrB₂:: MoSi₂=7:3:2 for ZSM; ZrB₂::MoSi₂=7:3 for ZS) were filled into the ZrO₂ jar and

ball milled for 6 h using ZrO₂ media. Subsequently, the slurries were dried in a rotary evaporator. The dried powder mixtures were filled into a graphite die, which was then put into the SPS furnace under argon atmosphere to sinter for 5 min at 1900 °C, with a heating rate of 100 °C/min and an applied pressure of 30 MPa.

II. RESULTS AND DISCUSSION

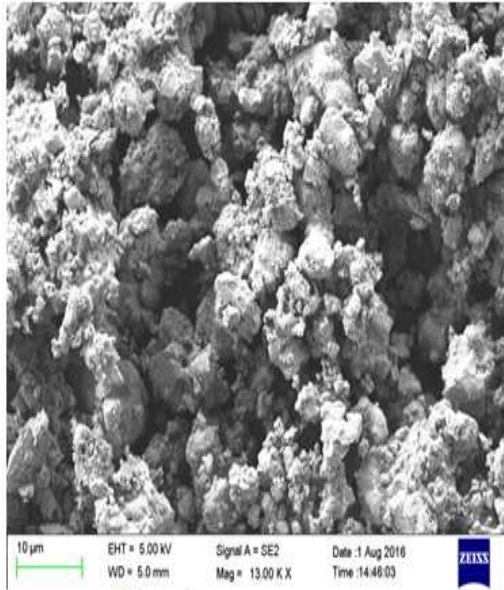


Figure 1. a

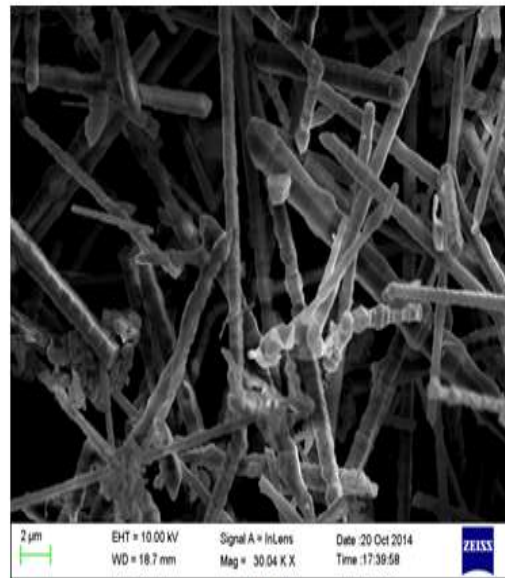


Figure 1. b

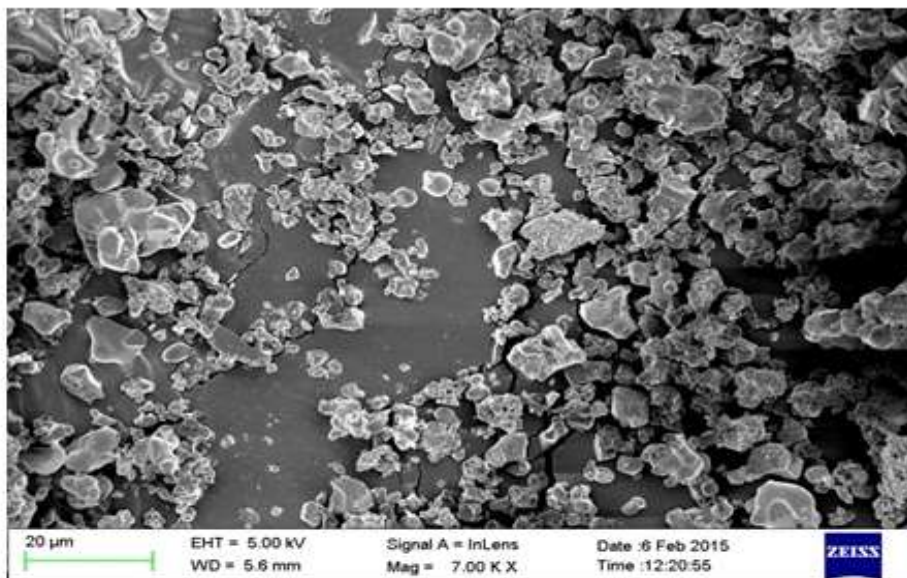


Figure 1. C

Figure 1. a SEM image of at 13000X Figure 1. b SEM image of SiC-Wat 3040X Figure 1.c SEM image of ZrB₂ at 7000X

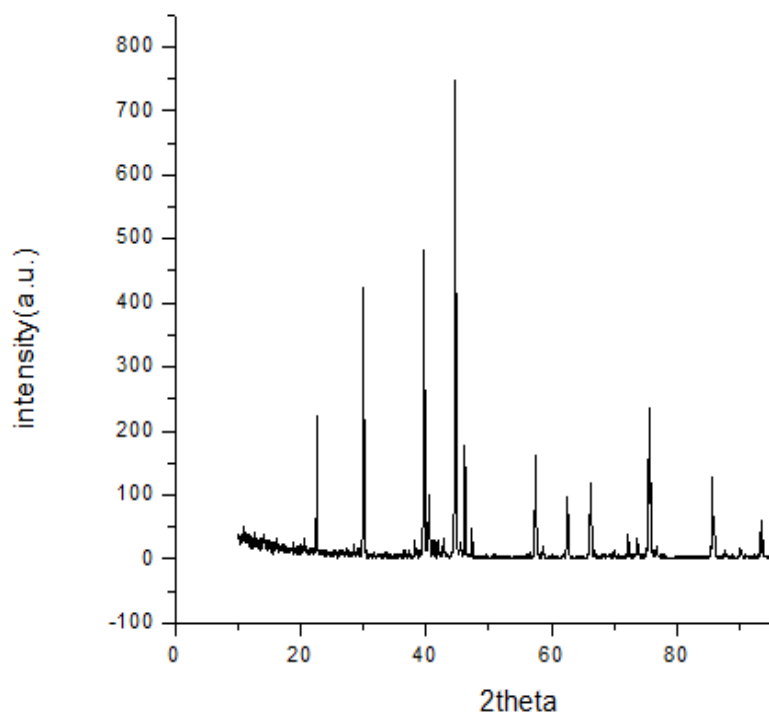


Fig 2.a X-Ray Diffractogram of MoSi₂

a = 0.32112 nm, b = 0.32112 nm,
 c = 0.45236 nm

| 2theta | (hkl) |
|--------|-------|
| 22.98 | 0 0 2 |
| 29.98 | 1 0 1 |
| 39.66 | 1 1 0 |
| 44.635 | 1 0 3 |
| 46.38 | 0 0 4 |
| 47.252 | 1 1 2 |
| 57.512 | 2 0 0 |
| 62.48 | 2 0 2 |
| 66.58 | 1 0 5 |
| 75.36 | 2 1 3 |
| 85.62 | 2 2 0 |
| 99.079 | 3 1 0 |

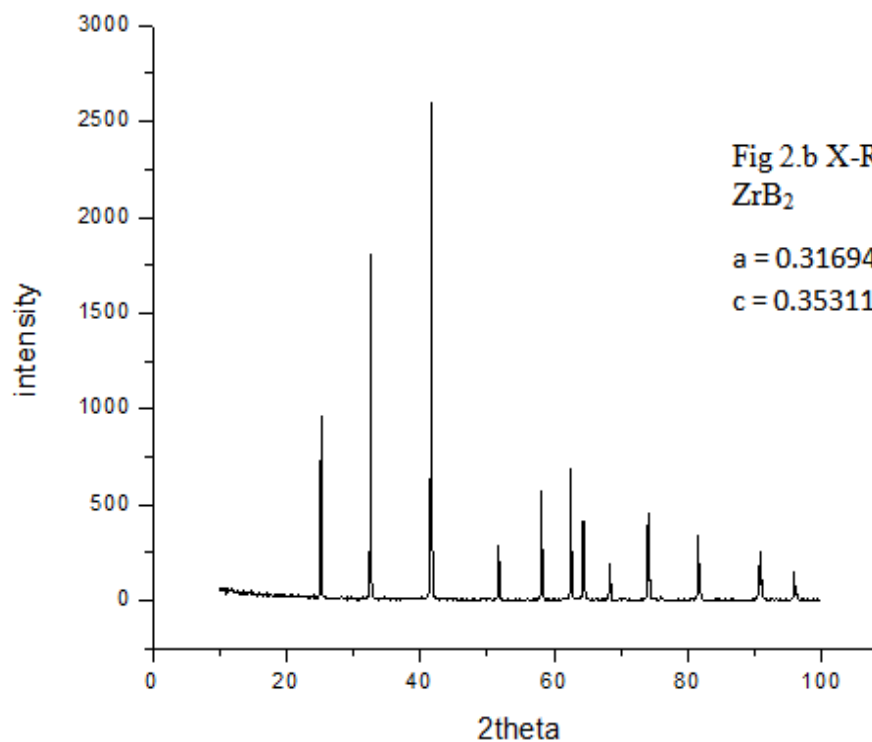
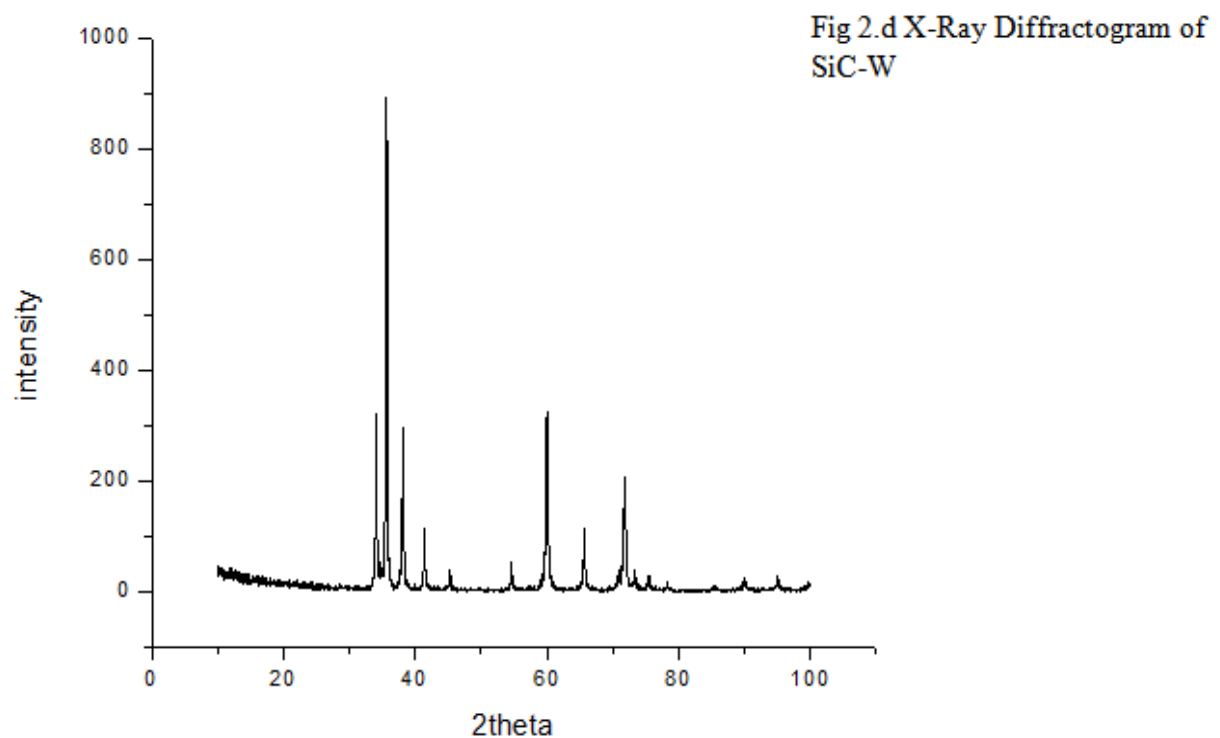
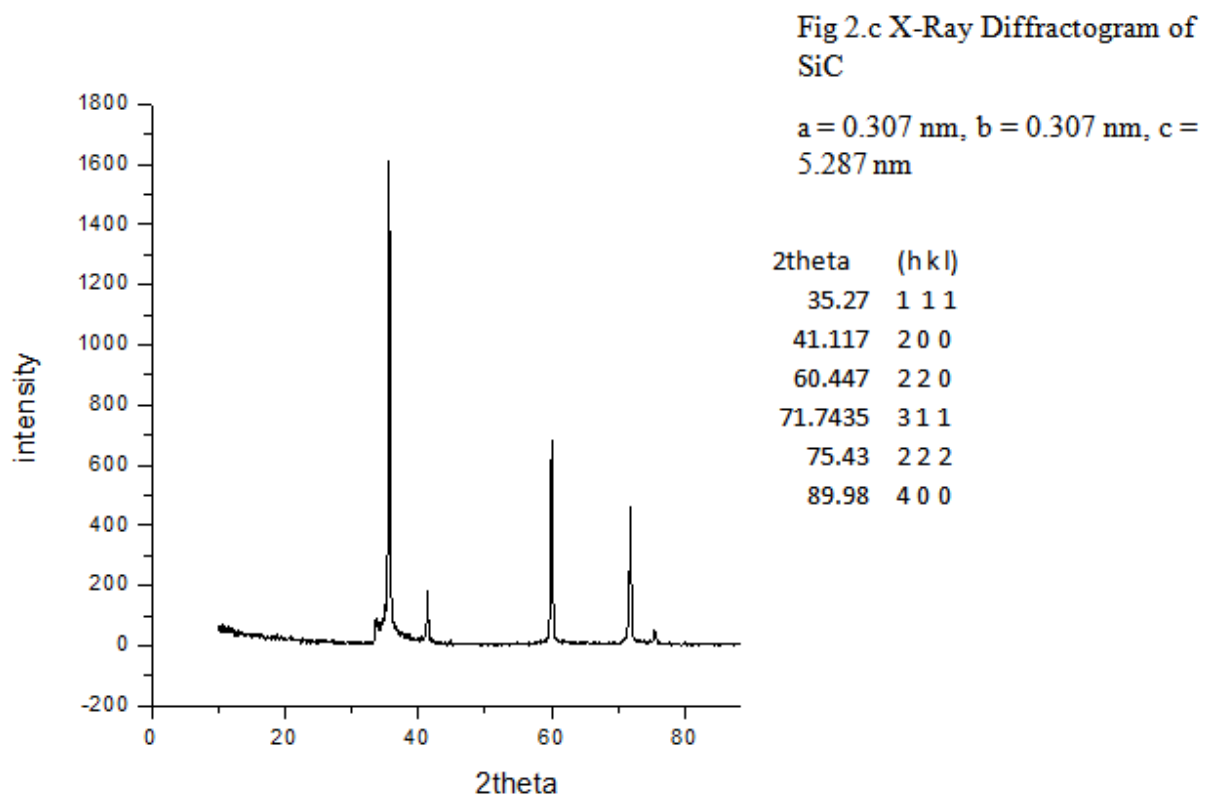


Fig 2.b X-Ray Diffractogram of ZrB₂

a = 0.31694 nm, b = 0.31694 nm,
 c = 0.35311 nm

| 2theta | (hkl) |
|--------|----------|
| 25.596 | 0 0 1 |
| 32.38 | 1 0 -1 0 |
| 41.69 | 1 0 -1 1 |
| 51.35 | 0 0 2 |
| 58.38 | 1 1 -2 0 |
| 62.77 | 1 0 -1 2 |
| 64.254 | 1 1 -2 1 |
| 68.036 | 2 0 -2 0 |
| 73.906 | 2 0 -2 1 |
| 81.52 | 1 1 -2 2 |
| 91.17 | 1 0 -1 3 |
| 95.85 | 2 1 -3 0 |



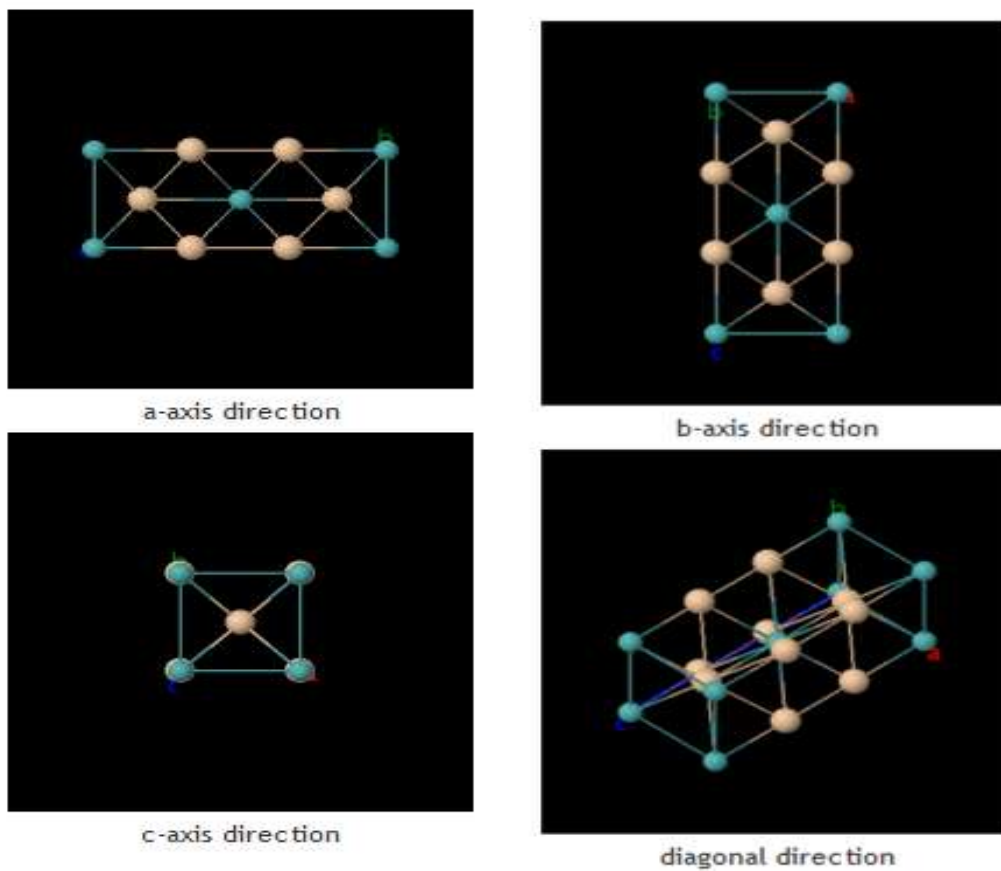


Fig 3 Tetragonal structure of MoSi_2 (Courtesy: NIST, Japan)

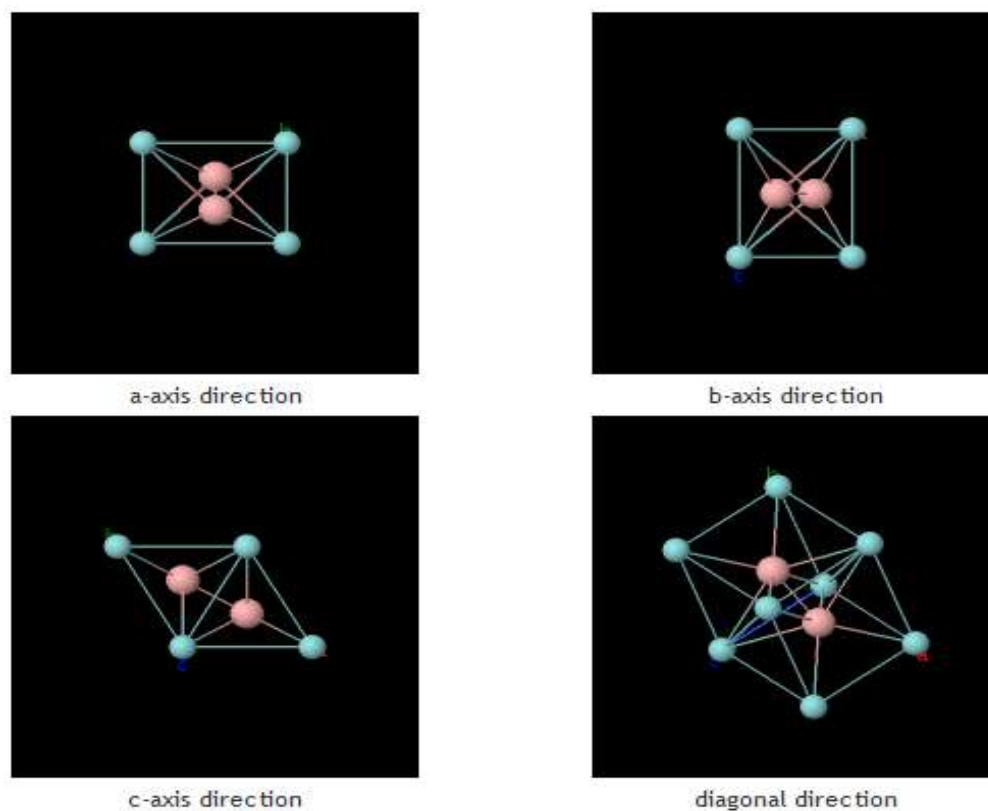


Fig 4. HCP structure of ZrB_2 (Courtesy: NIST, Japan)

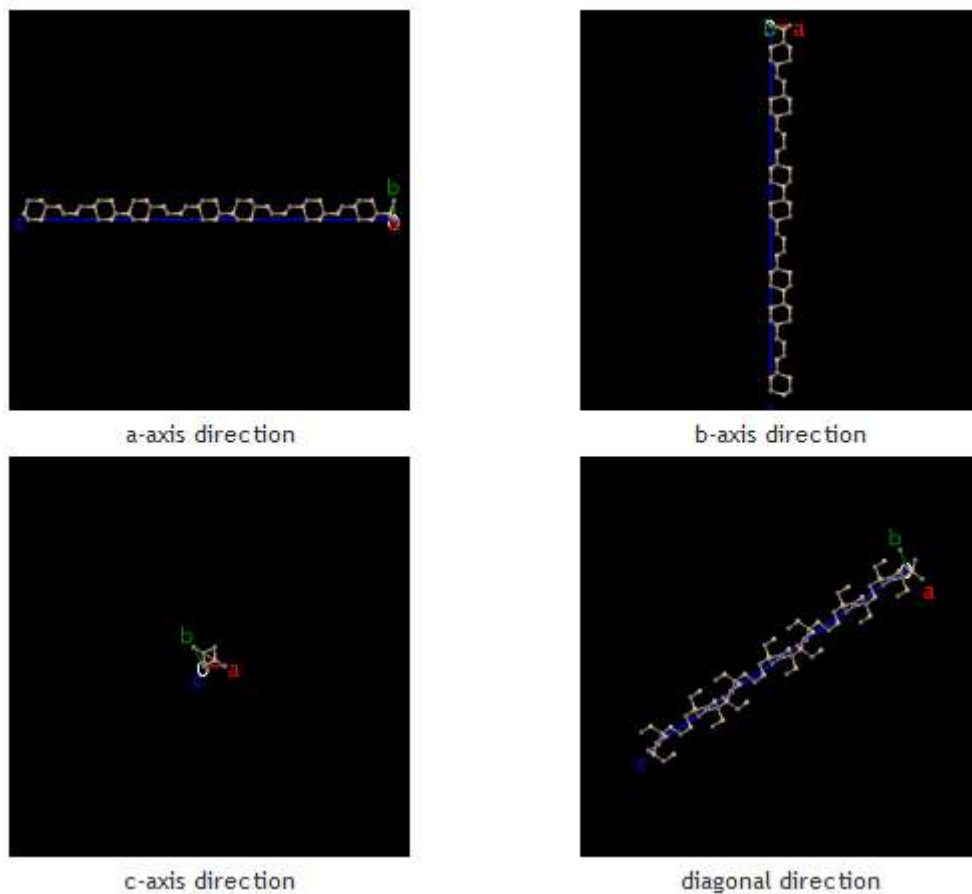


Fig 5. HCP structure of (Courtesy: NIST, Japan)

Table 1. Table for calculating microstructural features of MoSi₂ particles (dimensions: μm, using imageJ software)

| Count | Total Area | Avg % Area | % Area Mean | Median | mean Average Size | median |
|-------|------------|------------|-------------|--------|-------------------|--------|
| | 0.406 | 40.511 | 255 | 255 | | |
| 3915 | 1588.667 | 0.406 | 40.511 | | 255 | 255 |

Table 2. Table for calculating microstructural features of ZrB₂ particles (dimensions: μm using imageJ software)

| Count | Total Area | Avg % Area | % Area Mean | Median | mean Average Size | median |
|-------|------------|------------|-------------|--------|-------------------|--------|
| | 0.406 | 40.511 | 255 | 255 | | |
| 3724 | 4665.027 | 1.253 | 34.41 | | 255 | 255 |

Table 3. Table for calculating microstructural features of particles (dimensions: μm using imageJ software)

| Count | Total Area | Avg % Area | % Area Mean | Median | mean Average Size | median |
|-------|------------|------------|-------------|--------|-------------------|--------|
| | 0.406 | 40.511 | 255 | 255 | | |
| 571 | 213.68 | 0.374 | 29.622 | | 255 | 255 |

Hypothesis

From spdf configuration of atoms

C: [He]2s² 2p²

B: [He]2s² 2p¹

Si: [Ne]3s² 3p²

Zr: [Kr]4d² 5s²

Mo: [Kr]4d⁵ 5s¹

Addition of MoSi₂ with ZrB₂-SiC is hypothesized to reduce the sintering temperature for Spark Plasma

Sintering (SPS) as compared to that for ZrB₂-SiC due to presence of unpaired electron each in Zr and Mo atoms after hybridization. As a result, the 2 unpaired electrons may pair up with each other, thus, making the system more reactive for sintering from atomistic point of view.

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