

Heat transfer and blood flow in Arterioles: A Mathematical study

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ABSTRACT

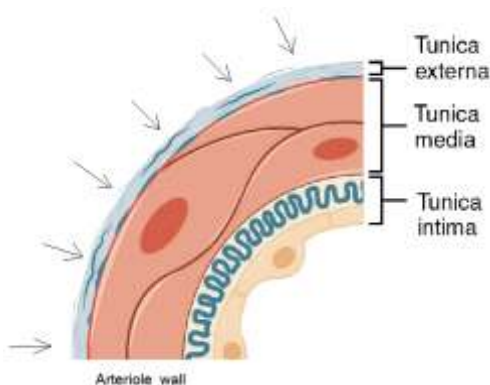
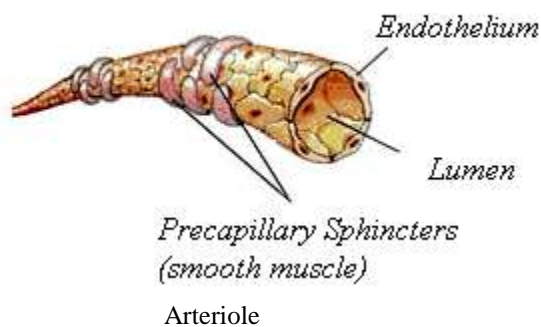
Blood flow is a study of measuring of the blood pressure and finding the flow through the blood vessel. In human body the arterioles have the greatest collective influence on both local blood flow and on the over all blood pressure. They are primary “adjustable nozzles” in the blood circulation system in human body, across which the greatest pressure drop occurs. In this paper a mathematical modeling of heat transfer through arterioles during blood flow is presented which is derived from the Navier-Stock equations and some assumptions. A system of non linear differential equations for blood flow and heat transfer through cross sectional area of the arterioles was obtained. MATLAB programming techniques were adopted to solve the equations. The results obtained are very sensitive to the values of the initial conditions and this helps to explain the condition of hypertension.

Key words: Heat transfer, Arterioles, Hypertension, Blood Flow, Lumen.

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I. INTRODUCTION



The thermal interaction between living tissue and blood has been the subject of investigation since the pioneering work of Pennes[7]. Mitvalsky[8] obtained mean values of the Nussely number for diluted blood steadily flowing in a 10mm I.D. pipe. Ahuja and Hendee[9] made experimrnt with RBC-plasmasuspensions and canine blood. The experiment of charm et al.[10] was specifically designed to get informationabout the heat transfer coefficient in microcirculation.

In above investigations on this subject vessel tapering and wall distensibility were overlooked. Recent development in this subject indicates that the transport of thermal energy is most significant.

Arterioles are the smallest vessels of the arterial system, with a diameter of about 1/3 millimeter or smaller. They serve as the major determinant of blood pressure and blood flow to the individual organs. Arterioles have a much smaller diameter then arteries and thus provide significant resistance to the flow of blood. This resistance creates pressure in circulatory system. Pressure is required to provide adequate flow of blood to all parts of the body. Blood flow to individual organs can be regulated by controlling the diameter of the arterioles. Vasodilatation (the term vasodilation refers to the dilation or relaxation of the arterioles to allow more blood to an area) of an arteriole lowers the resistance and results in an increase in flow

through that particular arterioles. In this problem along with blood flow convective heat transfer is studied. The arteriole is assumed as a tapered and blood is assumed to be a Newtonian fluid and blood flow is assumed to be fully developed laminar flow. In order to model this problem, Navier-Stock equations in cylindrical coordinate system will be used to derive the governing equations that represent this problem.

Formulation of the governing equations.

We have adopted Yang, Zhang and Asada's[3] local arterial flow model. This includes the assumptions that blood is considered as the incompressible Newtonian fluid and the flow is laminar and axially symmetric. The model approach is to use the two dimensional Navier-Stock equations and continuity equation for a Newtonian and incompressible fluid in cylindrical coordinate (r,z,t):

$$\frac{\partial w}{\partial t} + u \frac{\partial w}{\partial r} + w \frac{\partial w}{\partial z} = -\frac{1}{\rho_b} \frac{\partial p}{\partial z} + \frac{\mu}{\rho_b} \left(\frac{\partial^2 w}{\partial r^2} + \frac{1}{r} \frac{\partial w}{\partial r} + \frac{\partial^2 w}{\partial z^2} \right) \quad \text{----- (1)}$$

$$\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial r} + w \frac{\partial u}{\partial z} = -\frac{1}{\rho_b} \frac{\partial p}{\partial r} + \frac{\mu}{\rho_b} \left(\frac{\partial^2 u}{\partial r^2} + \frac{1}{r} \frac{\partial u}{\partial r} + \frac{\partial^2 u}{\partial z^2} - \frac{u}{r^2} \right) \quad \text{----- (2)}$$

$$\frac{1}{r} \frac{\partial}{\partial r} (ru) + \frac{\partial w}{\partial z} = 0 \quad \text{----- (3)}$$

Heat transfer in arteriole wall is given by

$$\rho_w C \frac{\partial T}{\partial t} - \text{div} (k \cdot \text{grad} (T)) = h(T_{ext} - T) \quad \text{----- (4)}$$

Where:

u and w = Radial velocity component and axial velocity component respectively

p = Pressure of the blood

ρ_b = The constant blood density

r = Radial co-ordinate

z = Axial co-ordinate

μ =Viscosity of blood.

ρ_w =Arteriole wall density

C =Heat capacity of wall

K =Coefficient of heat conductivity

.h =Convective heat transfer coefficient

T_{ext} = External temperature

Here, the magnitude of radial velocity (u) is very less in comparison to the magnitude of axial velocity(w) i.e. $u \ll w$, variation of velocity gradient in z direction is less in comparison to velocity gradient in r direction. i.e.

$$\frac{\partial w}{\partial z} \ll \frac{\partial w}{\partial r} \text{ and } \frac{\partial u}{\partial r}, \frac{\partial^2 u}{\partial r^2}, \frac{\partial^2 u}{\partial z^2} \text{ also neglected,}$$

therefore eq.1 and 2 are reduced as

$$\frac{\partial p}{\partial z} = \frac{\mu}{r} \left(r \frac{\partial^2 w}{\partial r^2} + \frac{\partial w}{\partial r} \right) \quad \text{----- (5)}$$

$$-\frac{1}{\rho_b} \frac{\partial p}{\partial r} = 0 \quad \text{----- (6)}$$

It is seen that from eq. 6 the pressure gradient function z is a function of z(p=p(z)) only which caused the

motion of flow, therefore: $\frac{\partial p}{\partial z} = \frac{dp}{dz}$

The boundary conditions of blood flow in arteriole are as follows

$$\frac{\partial w}{\partial r} = 0 \quad r = 0 \quad \text{----- (7a)}$$

$$w = 0 \quad r = R(z) \quad \text{----- (7b)}$$

Boundary condition for heat equations are as follows

$$T=T_0 \quad z=0$$

T= Constant for r =R (Dirichlet condition:- temperature is specified at outer wall)

Equation (4) is solved using PDETOOL feature of MATLAB.

By applying the boundary conditions, maximum velocity at the center line 7(a) and no slip velocity at the wall (for finite velocity 7(b)), on eq. 5 the velocity profile of the blood through arteriole is shown as:

$$w = \left(\frac{dp}{dz} \right) \left(\frac{R^2 - r^2}{4\mu} \right) \text{ ----- (8)}$$

Sanjeev Kumar and Sanjeet Kumar[4] discussed the physical model of tapered artery. Here the geometry of of the arteriole (fig-1) is modeled mathematically as follows:

$$R(z)=R_1 -m(z+L); 0 \leq z \leq d_0 \text{ -----(9)}$$

- Where R(z) = Effective radius of tapered arteriole
- R₁ = The radius of untapered arteriole
- m= tan φ = The slope of tapered arteriole
- φ = Tapering angle

Flow rate: Flow rate for Newtonian fluid (blood) ids defined as:

$$Q = \int_0^R 2\pi wrdr \text{ ----- (10)}$$

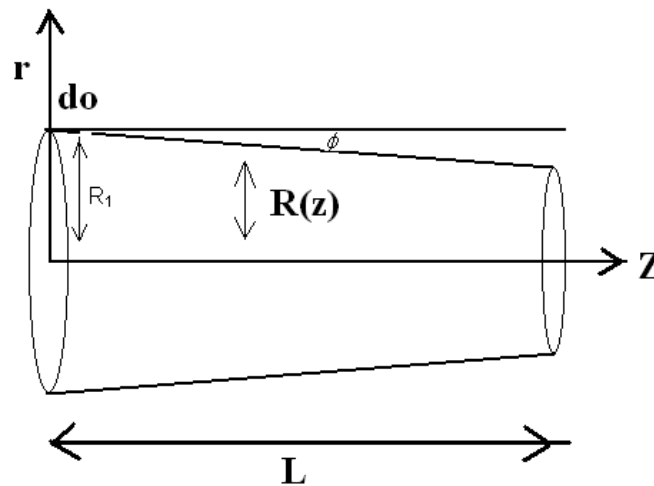


Figure -1

Fig-1 shows the physical model and co-ordinate.

Using eq. 8 into eq. 10, flow rate is shown as:

$$Q = \frac{\pi GR^4}{8\mu} \text{ ----- (11)}$$

Where G= $\frac{dp}{dz}$. Thus, the expression of total volumetric flow flux for tapered arteriole is shown as:

$$Q_L = \frac{\pi G}{8\mu} \int_0^L R^4 dz \text{ ----- (12)}$$

By using the geometry of fig-1 as shown in eq. 9 into eq. 12 the expression of non dimensional flow rate is shown as:

$$\bar{Q}_L = \frac{40 m \mu Q_L}{\pi G} A \text{ -----(13)}$$

Where $A = [(R_1 - mL)^5 - (R_1 - m(d_0 + L))^5]$

Wall shear stress: The constitutive relationship for the Newtonian fluid is given as

$$\lambda = \mu \left(- \frac{\partial w}{\partial r} \right) \text{ -----(14)}$$

From eq 5 and 11, the wall shear stress,

$$\tau_L = \frac{8 \mu Q}{\pi} \int_0^L R^{-3} dz \text{ ----- (15)}$$

Using eq.8 in 15 the expression of non dimensional wall shear stress

$$\bar{\tau}_L = \frac{m \pi \pi_L}{2Q \mu} A_1 \text{ ----- (16)}$$

Where $A_1 = \left[\frac{1}{(R_1 - m(d_0 + L))^2} - \frac{1}{(R_1 - mL)^2} \right]$

Resistance parameter: The resistance to flow λ (resistance parameter) is defined as follows:

$$\lambda = \frac{P_1 - P_0}{Q} \text{ -----(17)}$$

From eq 11 and using the conditions that the inlet pressure $p=p_1$ at $z=0$ and outlet pressure $p=p_0$ at $z=L$, the resistance parameter is shown as:

$$\lambda = \frac{8 \mu}{\pi} \int_0^L \frac{1}{R^4} dz \text{ -----(18)}$$

Thus the non dimensional resistance parameter $\bar{\lambda}$ for the tapered arteriole is given as

$$\bar{\lambda} = \frac{R_1^4}{3 mL} A_2$$

Where $A_2 = \frac{1}{[R_1 - m(d_0 + L)]^3} - \frac{1}{(R_1 - mL)^3}$

Results : Figure 1 and figure 2 show that flux and axial velocity increases with the radius of the for different tapering angles and figure 3 demonstrates the temperature variation in arteriole wall.

Table-1

Flux			
Radius(mm)	$\phi = 0^\circ$	$\phi = 1^\circ$	$\phi = 1^\circ 30'$
0.1	0.0000125	0.000015	0.000016
0.125	3.05176E-05	6.00E-05	8.60E-05
0.15	6.32813E-05	1.18E-04	1.89E-04
0.175	0.000117236	0.000225	0.000326
0.2	0.0002	0.000314	0.000436
0.225	0.000320361	0.00044	0.000574
0.25	0.000488281	0.00057	0.00077

Figure . 2 Plot of flux against radius of tapered arterioles for Newtonian flow

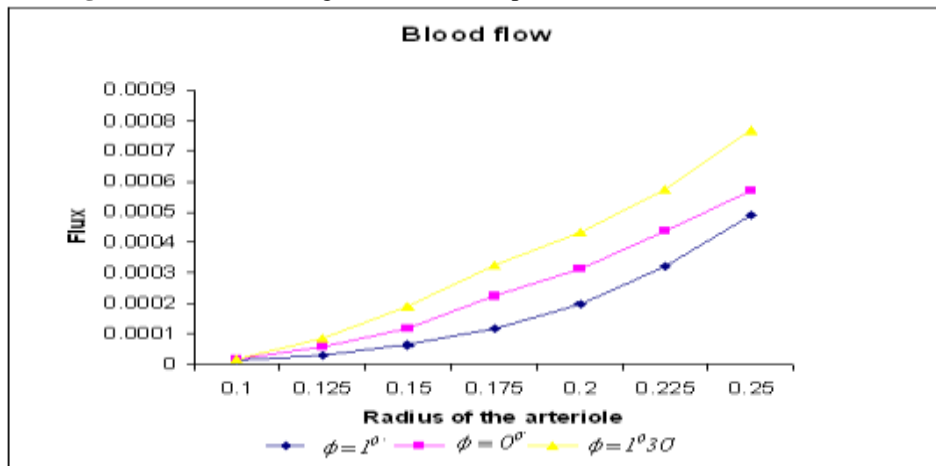


Table-2

Axial Velocity(for different tapering angles)				
Sl. No.	radius	$\phi = 0^\circ$	$\phi = 1^\circ$	$\phi = 1^\circ 30'$
1	0.1	0	0	0
2	0.125	0.034	0.04	0.07
3	0.15	0.055	0.0735	0.112
4	0.175	0.0712	0.103	0.136
5	0.2	0.0746	0.116	0.155
6	0.225	0.0742	0.1185	0.168
7	0.5	0.0709	0.1192	0.1827

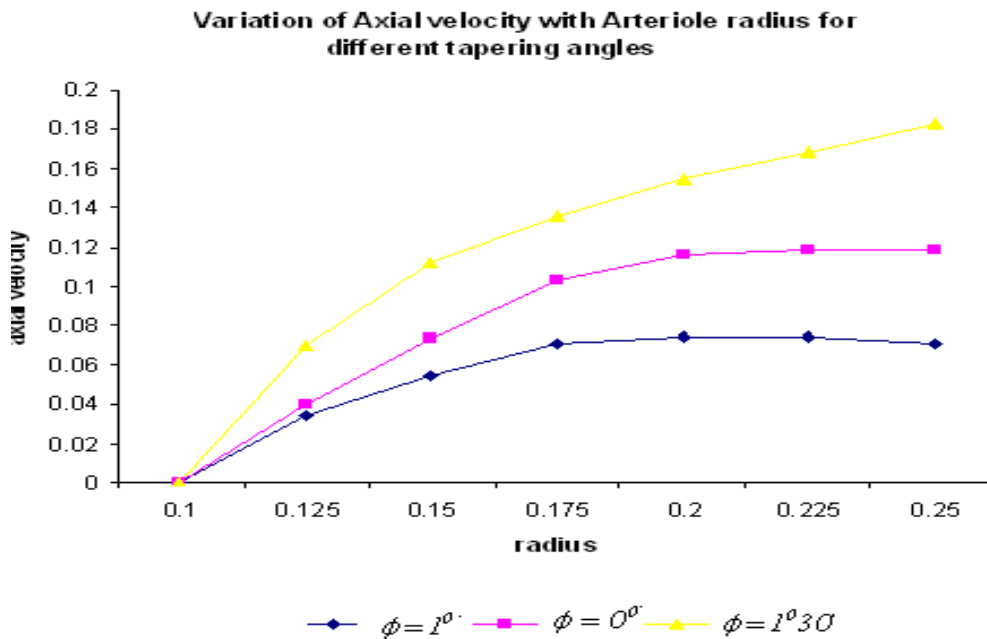


Figure-3

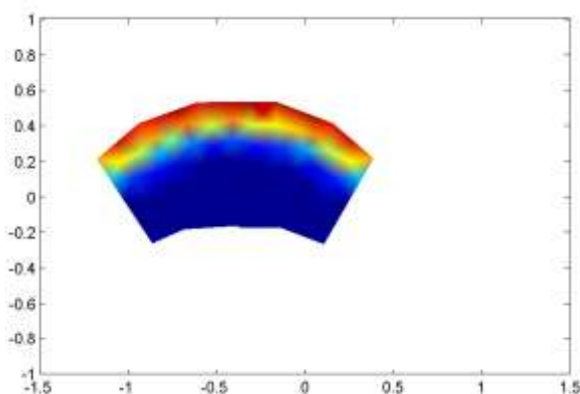


Figure-4 Temperature profile in arteriole wall

II. CONCLUSION

The flux, variation of axial velocity and temperature variation in arteriole wall are demonstrated in figure- 2, figure- 3 and figure- 4 respectively are obtained theoretically. These patterns have a close resemblance with the patterns obtained by simulation techniques[6].⁶. In the future, this study of blood flow and heat transfer in arterioles will lead to the prediction of individual hemodynamic flows in any patient, the development of diagnostic tools to quantify disease, and the design of devices that mimic or alter blood flow.

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