

## The Design and Performance Analysis of Refrigeration System Using R12 & R134a Refrigerants

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### ABSTRACT

The design and performance analysis of refrigeration system using R12 & R134a refrigerants are presented in this report. The design calculations of the suitable and necessary refrigerator equipment and their results are also reported here. CFC-12 is the most widely used refrigerant. It serves both in residential and commercial applications, from small window units to large water chillers, and everything in between. Its particular combination of efficiency, capacity and pressure has made it a popular choice for equipment designers. Nevertheless, it does have some ODP, so international law set forth in the Montreal Protocol has put CFC-12 on a phase out schedule. HFC-134a has been established as a drop-in alternative for CFC-12 in the industry due to their zero Ozone Depletion Potential (ODP) and similarities in thermodynamic properties and performance. However, when a system is charged with a HFC-134a compressor oil has to be changed. Not enough research has been done to cover all aspects of alternative refrigerants applications in the systems. This project intended to explore behavior of this alternative refrigerants compare to CFC-12 and challenges the industry is facing in design, operation services and maintenance of these equipments. The purpose of this project is to investigate behavior of R134a refrigerant. This includes performance and efficiency variations when it replaces R12 in an existing system as well as changes involved in maintaining the system charged with R134a. This project is intended to address challenges faced in the real world and some practical issues. Theoretical and experimental approaches used as a methodology in this work.

**Keywords** - alternate refrigerants, evaporator, HCFCs, ODP, GWP.

### I. INTRODUCTION

Refrigeration is concerned with the absorption of heat from where it is objectionable plus its transfer to and rejection at a place where it is unobjectionable. Regardless of means by which is heat transfer is accomplished; the problem is one of applied thermodynamics. In some methods of refrigeration the working medium that approaches perfect gases may be applied. A refrigerant is a compound used in a heat cycle that undergoes a phase change from a gas to a liquid and back. The two main uses of refrigerants are refrigerators/freezers and air conditioners. In broadest sense the word refrigerant is also applied to such secondary cooling medium as brine solutions, cooled water. The refrigerants include only those working mediums, which pass through the cycle or evaporation, recovery, compression and liquefaction.

### ANALYSIS OF VAPOUR COMPRESSION CYCLE DIAGRAM

The flow diagram T- $\phi$  and P-H diagrams of a vapour compression refrigerating system given below.



fig.1

### 1-2 ISENTROPIC COMPRESSION

Refrigerant vapour received from evaporator is compressed isentropically in a compressor by external source of energy

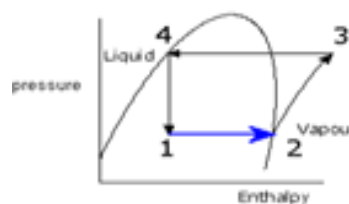


fig.2

(work in out), pressure and temperature increase.

## 2-3 CONDENSATION

Compressor discharges vapour into the condenser where it condensed completely i.e. turns into liquid. Heat is rejected from the refrigerant to cooling medium, usually air or water.

## 3-4 EXPANSION

From condenser liquid refrigerant passes through the expansion valve where it is throttled resulting in a drop of temperature and pressure. However, enthalpy remains constant (throttling expansion)

## 4-1 EVAPORATION

Liquid refrigerant at a low temperature passes into evaporator where it extract heat from the product to be cooled. Due to absorption of extract heat liquid refrigerant turns into vapour, and enters in to the compressor.

## COEFFICIENT OF PERFORMANCE

$$\text{Work input } W = H_2 - H_1$$

$$\text{Refrigerating effect } N = H_1 - H_4$$

Since, during the process 3-4, enthalpy is constant. Therefore enthalpy at 4(H4) is equal to enthalpy at 3(H3)

$$\text{Refrigerating effect } N = H_1 - H_3$$

$$\text{C.O.P} = \frac{\text{REF EFFECT}}{\text{WORK INPUT}} = \frac{H_1 - H_3}{H_2 - H_1}$$

## II. DETAILS OF DESIGN AND CONSTRUCTION

### SELECTION OF COMPRESSOR

#### Compressor specifications

Motor H.P.=1 H.P.

Speed= 640 r.p.m

#### Cylinder specifications

No of cylinders = 1

Bore diameter = 63.5 mm

Stroke length = 762 mm, Displacement = 4825 cm<sup>3</sup>

### DETAILS OF DESIGN EVAPORATOR

The selected evaporator for the design is natural convection bare tube, Dry Expansion, Shell and tube Evaporators.

Heat reaches the Evaporator by all three methods of heat transfer and conduction and radiation.

### DESIGN OF EVAPOURATOR

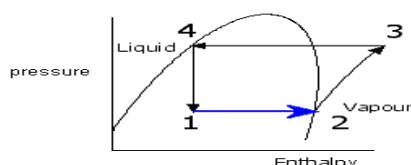


fig.4

Inlet temperature of the evaporator coil ( $T_1$ ) = -1.6°C

Outlet temperature of evaporator coil ( $T_2$ ) = 3.4°C

Temperature difference between inside and outside of the evaporator = (3.4)+(1.6) = 5

The overall heat transfer, co-efficient “U” factor from data tables for copper = 400kcal/m<sup>2</sup>-hr-°C

Load taken by the evaporator = AU ΔT

i.e. Refrigerating capacity = AU ΔT

Refrigerating capacity = load taken by Evaporator = 1555 = AU ΔT

$$A = 1555 / U \Delta T = 1555 / (400 \times 5) = 0.77 \text{ m}^2$$

Diameter of the coil (D) = 5mm

$$\text{Then } A = \pi DL$$

$$\text{Length of the coil (L)} = A / \pi D = 0.77 / (\pi \times 0.005) = 49.5 \text{ m}^2$$

$$\text{Length of coil in one turn} = 2(40+20)$$

$$= 180 \text{ cm}$$

$$\text{Number of turns in the tank} = 4950 / 180$$

$$= 27.4 \text{ turns, say 28 turns}$$

Provide 10 cm gap between each turn of the coil. The evaporator coil should be arranged the side of the tank that will be easy for periodic cleaning.

### SELECTION OF CONDENSER

The condenser load can be calculated by the following equation:

$$\text{Heat transfer } Q = m C_{pl} (T_3 - T_2)$$

$$\text{Load on the condenser} = m C_{pl} (T_3 - T_4)$$

Q = heat absorbed in evaporator + heat of compressor.

$$\text{Heat absorbed in evaporator} = 1555 \text{ k cal/h}$$

$$\text{Heat of compressor} = v \times 1$$

$$= 220 \times 3$$

$$= 640 \text{ w}$$

$$= 640 \times 0.86$$

$$= 550.4 \text{ kcal.}$$

$$Q = 1555 + 550.4 = 2105.4 \text{ k cal}$$

$$Q = UA \Delta T$$

$$A = 2105.4 / 400 \times 22$$

$$= 0.239$$

$$A = \pi dl$$

$$d = 5 \text{ mm}$$

$$\text{Length of coil (L)} = 0.239 / 0.005$$

$$= 15.23 \text{ m}$$

$$\text{LENGTH IN ONE TURN} = (40 + 40) = 80 \text{ cm}$$

$$\text{Number of turns required} = 15.23 / 0.80$$

$$= 19.0389$$

$$= 20$$



fig 5.Experimental Set-up

### III. STEPS FOR CONVERTING R-12 TO R-134A REFRIGERATOR

- Replace the compressor.
- Flush the entire system clean with alcohol and let it be free for few hours.
- Then rinse it with alcohol again and then blew it clean with DRY AIR (if you don't have a good air dryer for your compressor (or have no compressor), get a good compressed air).
- Replace all seals on the spring clamp and screw-together.
- Put the required amount of lubricating oil in the compressor.
- Charge with the new R134A refrigerant

### CALCULATIONS

Evaporator Temperature ( $T_1$ ) =  $-30^\circ\text{C}$   
 Condenser Temperature ( $T_2^1$ ) =  $30^\circ\text{C}$

From charts,

At  $-30^\circ\text{C}$ , Enthalpy ( $h_1$ ) = 338.143 kJ/kg  
 Entropy ( $s_1$ ) = 1.57507 kJ/ (kg.K)  
 At  $30^\circ\text{C}$ , Enthalpy ( $h_2^1$ ) = 363.566 kJ/kg  
 Entropy ( $s_2^1$ ) = 1.54334 kJ/ (kg.K)  
 Enthalpy ( $h_3$ ) = 228.540 kJ/kg

From the graph,

$$s_1 = s_2 \text{ and } h_3 = h_4$$

We know that,

$$h_2 = h_2^1 + C_p (T_2 - T_2^1)$$

Equation – A

$$s_2 = s_2^1 + C_p \ln (T_2/T_2^1)$$

$$1.57507 = 1.54334 + 0.7253 * \ln (T_2/303)$$

On simplification we get,  $T_2 = 316.5 \text{ K}$

Substituting in Equation – A we have,

$$h_2 = 363.566 + 0.7253 * (316.5 - 303) = 373.35 \text{ kJ/kg}$$

$$(1)\text{Refrigerating Effect} = h_1 - h_4 = 109.603 \text{ kJ/kg}$$

$$(2)\text{Coefficient of Performance (C.O.P)} = \frac{\text{Refrigerating Effect}}{\text{Work done by the Compressor}} = \frac{(h_1 - h_4)}{(h_2 - h_1)} = 3.11$$

### IV. RESULTS & DISCUSSIONS:

Graphs are drawn from the above tabulated results.

- Coefficient of Performance with Evaporator Temperature at a constant Condenser Temperature.
- Compressor exit Temperature with Evaporator Temperature at a constant Condenser Temperature.
- Specific Volume at inlet to Compressor with Evaporator Temperature.

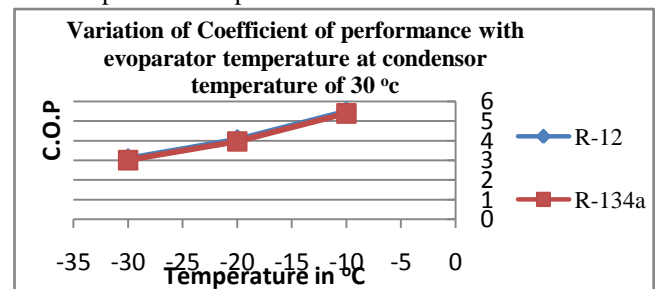


fig.6 Variation of C.O.P with evaporator temp.at condenser temperature of  $30^\circ\text{C}$

From the Fig.6 It is observed that the coefficient of performance of the refrigeration system is increasing almost linearly as the Evaporator Temperature is increased when the refrigerant used was R-12. The shape of the graph is almost similar when the results were plotted using R-134a as the refrigerant however it is observed that the values of coefficient of performance are slightly higher in case of refrigerants R-12. But refrigerant are R-134a may be preferred because of the zero value of the ozone depletion potential.

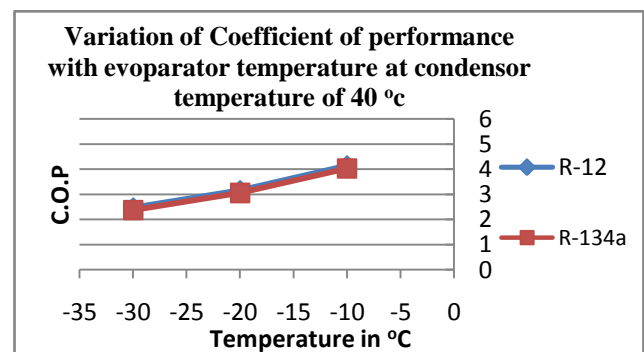


fig.7 Variation of C.O.P with evaporator temp.at condenser temperature of  $40^\circ\text{C}$

From the fig.7 It is observed that the coefficient of performance of the refrigeration system is increasing almost linearly as the Evaporator Temperature is increased when the refrigerant used was R-12. The shape of the graph is almost similar when the results were plotted using R-134a as the refrigerant however it is observed that

the values of coefficient of performance are slightly higher in case of refrigerants R-12. But refrigerant are R-134a may be preferred because of the zero value of the ozone depletion potential

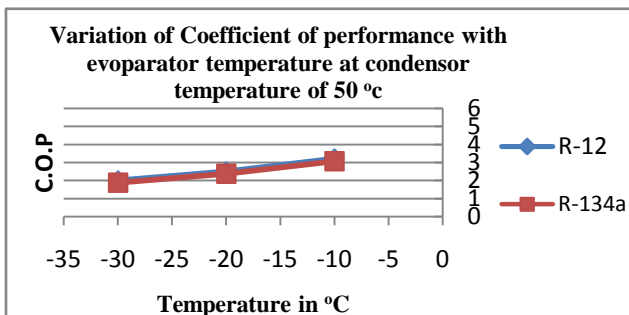


fig.8 Variation of C.O.P with evaporator temp. at condenser temperature of 50°C

From fig.8 It is observed that the coefficient of performance of the refrigeration system is increasing almost linearly as the Evaporator Temperature is increased when the refrigerant used was R-12. The shape of the graph is almost similar when the results were plotted using R-134a as the refrigerant however it is observed that the values of coefficient of performance are slightly higher in case of refrigerants R-12. But refrigerant are R-134a may be preferred because of the zero value of the ozone depletion potential

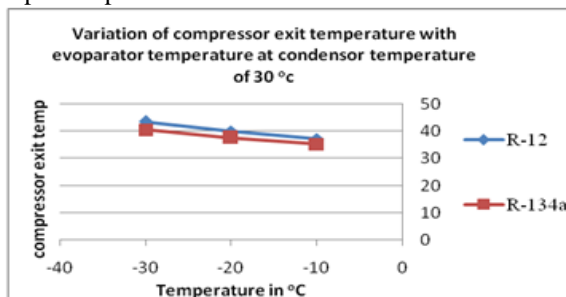


fig.9 Variation of Compressor Exit Temperature with evaporator temp. at condenser temperature of 30°C

From fig.9 it is observed that the compressor exit Temperatures keeping the Condenser Temperature constant at 30°C the Evaporator Temperature is varied from -30°C to -10°C at intervals of 10°C it is absorbed that from the graph the compressor Temperature as the Evaporator Temperature is increased from -10°C to -30 °C . In case of R-134a the shape of the graph is similar in case R-12.

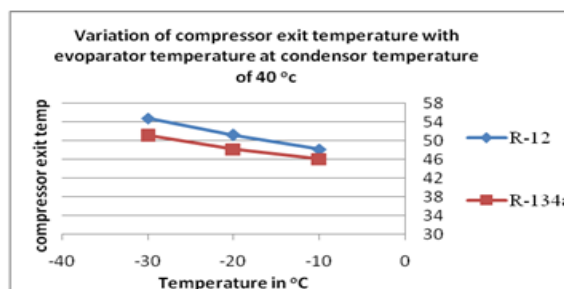


fig.10 Variation of Compressor Exit Temperature with evaporator temp. at condenser temperature of 40°C

From fig.10 it is observed that the compressor exit Temperatures keeping the Condenser Temperature constant at 40°C the Evaporator Temperature is varied from -30°C to -10°C at intervals of -10°C it is absorbed that from the graph the difference in the Compressor exit temperature between R-12 & R-134a is more at an Evaporator Temperature of -30 and is relatively less when the Evaporator Temperature is -10°C .

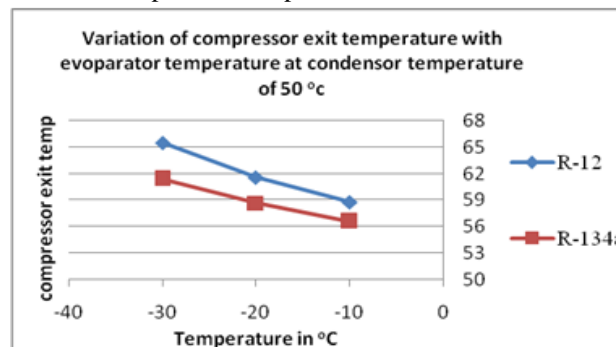


fig.11 Variation of Compressor Exit Temperature with evaporator temp. at condenser temperature of 50°C

From fig.11 it is observed that the compressor exit Temperatures keeping the Condenser Temperature constant at 50°C the Evaporator Temperature is varied from -30°C to -10°C at intervals of -10°C it is absorbed that from the graph the difference in the Compressor exit temperature between R-12 & R-134a is more at an Evaporator Temperature of -30°C and is relatively less when the Evaporator Temperature is -10°C

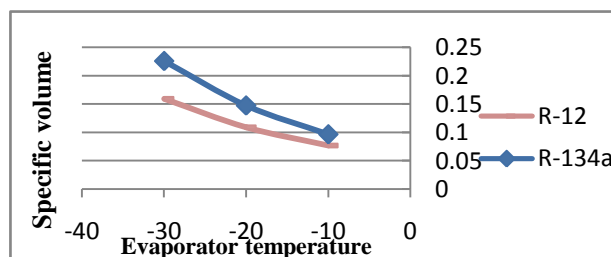


fig.12 Variation of specific volume with evaporator temperature

According to the graph fig.12 the specific volume is plotted against Evaporator Temperature it is observed that the difference in specific volume between R-12 & R-134a is less at an evaporator Temperature of  $-30^{\circ}\text{C}$  and is relatively less when the Evaporator Temperature is  $-10^{\circ}\text{C}$ .

From the graphs, we know that Coefficient of Performance for R-12 refrigerant is slightly greater than that of R-134a refrigerant. Even though the C.O.P for R-12 refrigerant is slightly greater than that of R-134a refrigerant, we prefer to use R-134a refrigerant because its Ozone Depletion Potential value is zero. Also, the replacement of CFCs with HFCs provides more efficient refrigeration and does not act as greenhouse gas and the less electricity is needed for refrigeration.

## V. CONCLUSION

It has been observed that the refrigerator test rig is very much suitable for educational purposes. In order to know working of VCR system practically and also for knowing the pressure and temperatures at various points of the cycle. These results will help for modifications and for new designs. It has been seen from the results and graphs that COP of R12 is little greater than COP of R134a. Even though COP of R12 is greater than R134a it must be replaced with R134a because of following reasons.

- R134a refrigerant is non-toxic and does not flare up within the whole range of operational temperatures.
- Ozone depletion potential ODP=0, global warming potential GWP=0.25 and Estimated Atmospheric life EAL=16.
- In Middle temperature refrigeration facilities and air conditioning systems, refrigerating factor of R134a is equal to the factor for R12 or higher than that.
- In high temperature refrigeration facilities, specific cold-productivity when operating on R134a is also a bit higher than that of R12.
- Increasing of dehumidifying ability of filter dehydrators due to high hygroscopic property of R134a system-synthetic oil.
- Improvement of widely used all over the world as a main substitute of R12 for refrigeration equipment operating within middle-temperature range. It is used in automobile air-conditioners, domestic refrigerators, commercial refrigeration middle-temperature equipment, industrial facilities, air-conditioning systems in building and industrial areas, as well as on refrigeration transport.
- As R134a molecule has smaller size than R12 molecule which makes danger of leakage, this can be avoided by using suitable materials, in particular, with pads, made of such materials as

“Buna-N”, “Khailaon”, “Neopren”, “Nordel” which are more compatible with R134a.

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