

Improvement of Dynamic Stability of a SMIB using Fuzzy Logic Based Power System Stabilizer

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ABSTRACT

Power systems are subjected to low frequency disturbances that might cause loss of synchronism and an eventual breakdown of entire system. The oscillations, which are typically in the frequency range of 0.2 to 3.0 Hz, might be excited by the disturbances in the system or, in some cases, might even build up spontaneously. These oscillations limit the power transmission capability of a network and, sometimes, even cause a loss of synchronism and an eventual breakdown of the entire system. For this purpose, Power system stabilizers (PSS) are used to generate supplementary control signals for the excitation system in order to damp these low frequency power system oscillations.

The use of power system stabilizers has become very common in operation of large electric power systems. The conventional PSS which uses lead-lag compensation, where gain settings designed for specific operating conditions, is giving poor performance under different loading conditions. The constantly changing nature of power system makes the design of CPSS a difficult task. Therefore, it is very difficult to design a stabilizer that could present good performance in all operating points of electric power systems. To overcome the drawback of conventional power system stabilizer (CPSS), many techniques such as fuzzy logic, genetic algorithm, neural network etc. have been proposed in the literature.

In an attempt to cover a wide range of operating conditions, Fuzzy logic Based technique has been suggested as a possible solution to overcome the above problem, thereby using this technique complex system mathematical model can be avoided, while giving good performance under different operating conditions. Fuzzy Logic has the features of simple concept, easy implementation, and computationally efficient. The fuzzy logic based power system stabilizer model is evaluated on a single machine infinite bus power system, and then the performance of Conventional power system stabilizer (CPSS) and Fuzzy logic based Power system stabilizer (FLPSS) are compared. Results presented in the thesis demonstrate that the fuzzy logic based power system stabilizer design gives better

performance than the Conventional Power system stabilizer.

Keywords -Generator Excitation System, Synchronous Machine Model, Automatic Voltage Regulator (AVR), Power System Stabilizer, Fuzzy Logic Controller (FLC), PID, Controller Design, Robust control.

I. INTRODUCTION

Power system stability is the tendency of a power system to develop restoring forces equal to or greater than the disturbing forces to maintain the state of equilibrium. Since power systems rely on synchronous machines for generation of electrical power, a necessary condition for satisfactory system operation is that all synchronous machines remain in synchronism. This aspect of stability is influenced by the dynamics of generator rotor angles and power-angle relationships. The power system is a dynamic system. The electrical power systems today are no longer operated as isolated systems, but as interconnected systems which may include thousands of electric elements and be spread over vast geographical areas. There are many advantages of interconnected power systems.

The power system is a dynamic system. It is constantly being subjected to disturbances, which cause the generator voltage angle to change. When these disturbances die out, a new acceptable steady state operating condition is reached. It is important that these disturbances do not drive the system to unstable condition. The disturbances may be of local mode having frequency range of 0.7 to 2 Hz or of inter area modes having frequency range in 0.1 to 0.8 Hz, these swings are due to the poor damping characteristics caused by modern voltage regulators with high gain. A high gain regulator through excitation control has an important effect of eliminating synchronizing torque but it affects the damping torque negatively. To compensate the unwanted effect of these voltage regulators, additional signals are introduced in feedback loop of voltage regulators. The additional signals are mostly derived from speed deviation, excitation deviation or accelerating power. This is achieved by injecting a stabilizing signal into the excitation system voltage reference summing point junction. The device setup

to provide this signal is called “power system stabilizer”.

Excitation control is well known as one of the effective means to enhance the overall stability of electrical power systems. Present day excitation systems predominantly constitute the fast acting AVRs. A high response exciter is beneficial in increasing the synchronizing torque, thus enhancing the transient stability i.e. to hold the generator in synchronism with power system during large transient fault condition. However, it produces a negative damping especially at high values of external system reactance and high generator outputs.

Stability of synchronous generators depends upon number of factors such as setting of automatic voltage regulators (AVR). AVR and generator field dynamics introduces a phase lag so that resulting torque is out of phase with both rotor angle and speed deviation. Positive synchronizing torque and negative damping torque often result, which can cancel the small inherent positive damping torque available, leading to instability.

Generator excitation controls have been installed and made faster to improve stability. PSS have been added to the excitation systems to improve the oscillatory instability it is used to provide a supplementary signal to excitation system. The basic function of PSS is to extend the stability limit by modulating generator excitation to provide the positive damping torque to power swing modes.

The application of power system stabilizer (PSS) is to generate a supplementary signal, which is applied to control loop of the generating unit to produce a positive damping. The most widely used conventional PSS is lead-lag PSS where the gain settings are fixed under certain value which are determined under particular operating conditions to result in optimal performance for a specific condition. However, they give poor performance under different synchronous generator loading conditions.

II. SYSTEM MODELING

The Mathematical Models needed for small signal analysis of Synchronous Machines, Excitation System and lead-lag power system stabilizer are briefly reviewed. The Guidelines for the selection of Power System Stabilizer parameters are also presented.

i. Synchronous Machine Model

The synchronous machine is vital for power system operation. The general system configuration of synchronous machine connected to infinite bus through transmission network can be represented as the mathematical models needed for small signal analysis of synchronous machine; excitation system and the lead-lag power system stabilizer are briefly reviewed. The guidelines for the selection of power

system stabilizer parameters are also presented. The Thevenin's equivalent circuit shown in Fig. 1.1

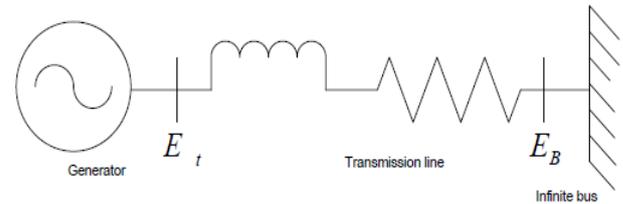


Fig. 1.1 The equivalent circuit of synchronous machine connected to infinite bus.

ii. Classical System Model

The generator is represented as the voltage E' behind X_d' as shown in Fig. 1.2. The magnitude of E' is assumed to remain constant at the pre-disturbance value. Let δ be the angle by which E' leads the infinite bus voltage E_B . The δ changes with rotor oscillation. The line current is expressed as –

$$I_t = \frac{E' \angle 0^\circ - E_B \angle -\delta}{jX_T} = \frac{E' - (E_B \cos \delta - j \sin \delta)}{jX_T} \quad (1)$$

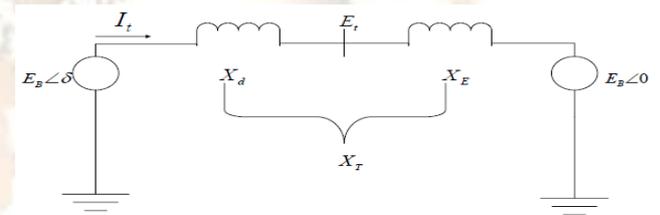


Fig. 1.2: Classical model of generator

The Complex Power behind X_d' is given by-

$$S = P + jQ = \frac{E' E_B \sin \delta}{X_T} + j \frac{E' (E' - E_B \cos \delta)}{X_T} \quad (2)$$

With stator resistance neglected, the air-gap power (P_e) is equal to the terminal power (P). In per unit, the air-gap torque is equal to the air-gap power. Hence

$$T_e = P = \frac{E' E_B \sin \delta}{X_T} \quad (3)$$

Linearising about an initial operating condition represented by δ_0 yields

$$\Delta T_e = \frac{\partial T_e}{\partial \delta} \Delta \delta = \frac{E' E_B \cos \delta_0}{X_T} (\Delta \delta) = K_s \Delta \delta \quad (4)$$

Where, $K_s = \frac{E' E_B \cos \delta_0}{X_T}$

The equations of motion in per unit are:

$$p \Delta \omega_r = \frac{1}{2H} (T_M - T_e - K_D \Delta \omega_r) \\ p \delta = \omega_0 \Delta \omega_r \quad (5)$$

Linearising Eqn. 5 and substitute for ΔT_e , given by equation 4, result into:

$$p \Delta \omega_r = \frac{1}{2H} (\Delta T_M - K_s \Delta \delta - K_D \Delta \omega_r) \\ p \Delta \delta = \omega_0 \Delta \omega_r \quad (6)$$

Writing equation 6 in Matrix form we obtain

$$\frac{d}{dt} \begin{pmatrix} \Delta\omega \\ \Delta\delta \end{pmatrix} = \begin{pmatrix} -\frac{K_D}{2H} & -\frac{K_s}{2H} \\ \omega_0 & 0 \end{pmatrix} \begin{pmatrix} \Delta\omega \\ \Delta\delta \end{pmatrix} + \begin{pmatrix} 1 \\ 0 \end{pmatrix} \Delta T_M \quad (7)$$

The equation 7 is of the form of $\dot{x} = Ax + Bu$. The elements of the state matrix A are seen to be dependent on the system parameters K_D , H, X_T , and the initial operating condition represented by the value of E' and δ_0 . The equation 7 to describe small-signal performance is represented in block diagram as Fig. 1.3

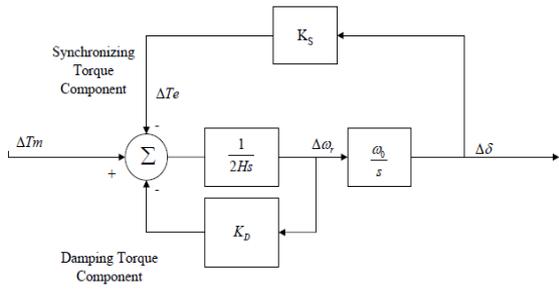


Fig. 1.3: Block diagram of single machine infinite bus system with classical model

From the block diagram we have:

$$\begin{aligned} \Delta\delta &= \frac{\omega_0}{s} \left(\frac{1}{2Hs} (-K_s\Delta\delta - K_D\Delta\omega + \Delta T_M) \right) \\ &= \frac{\omega_0}{s} \left(\frac{1}{2Hs} (-K_s\Delta\delta - K_D\frac{\Delta\delta}{\omega_0}s + \Delta T_M) \right) \end{aligned} \quad (8)$$

Solving the block diagram we get the characteristics equation:

$$s^2 + \frac{K_D}{2H}s + \frac{K_s\omega_0}{2H} = 0 \quad (9)$$

Comparing it with general form, the undamped natural frequency ω_n and damping ratio ξ are expressed as –

$$\begin{aligned} \omega_n &= \sqrt{\frac{K_s\omega_0}{2H}} \\ \xi &= \frac{1}{2} \frac{K_D}{\sqrt{K_s 2H\omega_0}} \end{aligned} \quad (10)$$

III. POWER SYSTEM STABILIZER MODEL

The basic function of power system stabilizer is to add damping to the generator rotor oscillations by controlling its excitation using auxiliary stabilizing signals. To provide damping, the stabilizer must produce a component of electrical torque in phase with rotor speed deviations. The theoretical basis for PSS may be illustrated with the aid of block diagram as shown in Fig. 1.4

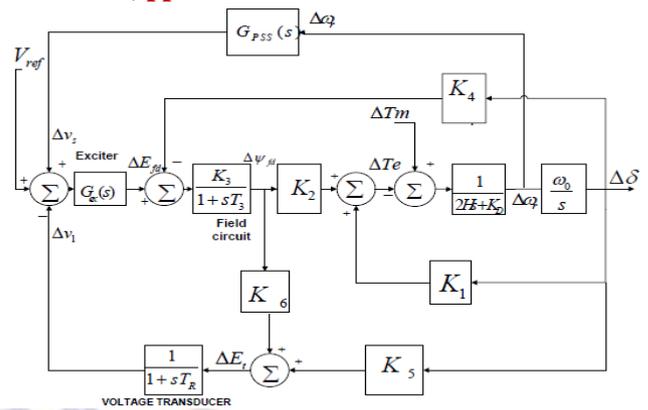


Fig. 1.4: Block diagram representation with AVR and PSS

Since the purpose of PSS is to introduce a damping torque component. A logical signal to use for controlling generator excitation is the speed deviation $\Delta\omega$. The PSS transfer function, $G_{PSS}(s)$, should have appropriate phase compensation circuits to compensate for the phase lag between exciter input and electrical torque. The following is a brief description of the basis for the PSS configuration and consideration in selection of parameters.

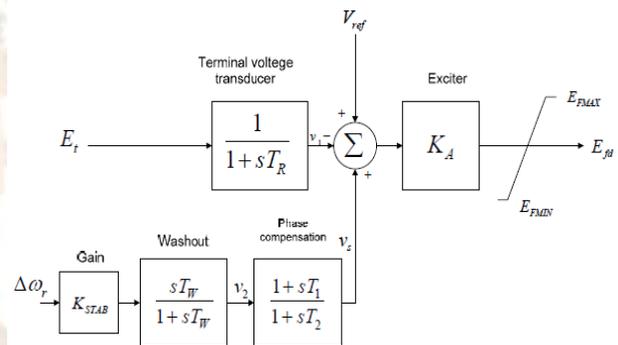


Fig. 1.5: Thyristor excitation system with AVR and PSS

The phase compensation block provides the appropriate phase lead characteristics to compensate for the phase lag between exciter input and generator electrical torque. The phase compensation may be a single first order block as shown in Fig. 1.5 or having two or more first order blocks or second order blocks with complex roots.

The signal washout block serves as high pass filter, with time constant T_w high enough to allow signals associated with oscillations in w_r to pass unchanged, which removes d.c. signals. Without it, steady changes in speed would modify the terminal voltage. It allows PSS to respond only to changes in speed.

The stabilizer gain K_{STAB} determines the amount of damping introduced by PSS. Ideally, the gain should be set at a value corresponding to maximum damping; however, it is limited by other consideration.

The PSS parameters should be such that the control

system results into the following-

- Maximize the damping of local plant mode as well as inter-area mode oscillations without compromising stability of other modes.
- Enhance system transient stability.
- Not adversely affect system performance during major system upsets which cause large frequency excursions; and
- Minimize the consequences of excitation system malfunction due to component failure.

IV. POWER SYSTEM STABILIZER MODEL

Fuzzy logic is a derivative from classical Boolean logic and implements soft linguistic variables on a continuous range of truth values to be defined between conventional binary i.e. [0, 1]. It can often be considered a subset of conventional set theory. The fuzzy logic is capable to handle approximate information in a systematic way and therefore it is suited for controlling non-linear systems and for modeling complex systems where an inexact model exists or systems where ambiguity or vagueness is common. It is advantageous to use fuzzy logic in controller design due to the following reasons –

- A Simpler and faster Methodology.
- It reduces the design development cycle.
- It simplifies design complexity.
- An alternative solution to non-linear control.
- Improves the control performance.
- Simple to implement.
- Reduces hardware cost.

i. FUZZY MEMBERSHIP

In classical set theory, a subset U of asset S can be defined as a mapping from the elements of S to the elements the subset {0, 1},

$$U: S \rightarrow \{0,1\}$$

The mapping may be represented as a set of ordered pairs, with exactly one ordered pair present for each element of S. The first element of the ordered pair is an element of the set S, and second element is an element of the set (0, 1). The value zero is used to represent non-membership, and the value one is used to represent complete membership. The truth or falsity of the statement 'X is in U' is determined by finding the ordered pair whose first element is X. The statement is true if the second element of the ordered pair is 1, and the statement is false if it is 0.

V. FUZZY CONTROLLER

The fuzzy control systems are rule-based systems in which a set of fuzzy rules represent a control decision mechanism to adjust the effects of certain system stimuli. With an effective rule base, the fuzzy control systems can replace a skilled

human operator. The fuzzy logic controller provides an algorithm which can convert the linguistic control strategy based on expert knowledge into an automatic control strategy. The Fig. 1.6 illustrates the schematic design of a fuzzy logic controller which consists of a fuzzification interface, a knowledge base, decision making logic, and a defuzzification interface.

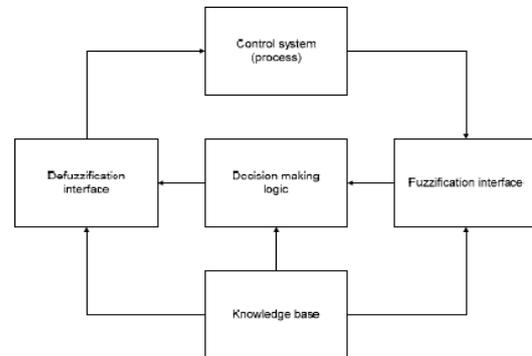


Fig. 1.6: The principle design of fuzzy logic controller

CONTROLLER DESIGN PROCEDURE

The fuzzy logic controller (FLC) design consists of the following steps.

- 1) Identification of input and output variables.
- 2) Construction of control rules.
- 3) Establishing the approach for describing system state in terms of fuzzy sets, i.e. establishing fuzzification method and fuzzy membership functions.
- 4) Selection of the compositional rule of inference.
- 5) Defuzzification method, i.e., transformation of the fuzzy control statement into specific control actions.

The above steps are explained with reference to fuzzy logic based power system stabilizer in the following section. Thus helps understand these steps more objectively.

VI. FUZZY LOGIC BASED PSS

The power system stabilizer is used to improve the performance of synchronous generator. However, it results into poor performance under various loading conditions when implemented with conventional PSS. Therefore, the need for fuzzy logic PSS arises. The fuzzy controller used in power system stabilizer is normally a two-input and a single-output component. It is usually a MISO system. The two inputs are change in angular speed and rate of change of angular speed whereas output of fuzzy logic controller is a voltage signal. A modification of feedback voltage to excitation system as a function of accelerating power on a unit is used to enhance the stability of the system.

i. SELECTION OF INPUT & OUTPUT VARIABLES

Define input and control variables, that is, determine which states of the process should be

observed and which control actions are to be considered. For FLPSS design, generator speed deviation and acceleration can be observed and have been chosen as the input signal of the fuzzy PSS. The dynamic performance of the system could be evaluated by examining the response curve of these two variables. The voltage is taken as the output from the fuzzy logic controller.

In Practice, only shaft speed is readily available. The acceleration signal can be derived from the speed signals measure at two successive instants using the following equations:

$$\Delta\omega(k) = \frac{((\Delta\omega(k) - \Delta\omega(k-1)))}{\Delta T}$$

ii. MEMBERSHIP FUNCTION

The variables chosen for this controller are speed deviation, acceleration and voltage. In this, the speed deviation and acceleration are the input variables and voltage is the output variable. The number of linguistic variables describing the fuzzy subsets of a variable varies according to the application. Usually an odd number is used. A reasonable number is seven. However, increasing the number of fuzzy subsets results in a corresponding increase in the number of rules. Each linguistic variable has its fuzzy membership function. The membership function maps the crisp values into fuzzy variables. The triangular membership functions are used to define the degree of membership. It is important to note that the degree of membership plays an important role in designing a fuzzy controller.

Each of the input and output fuzzy variables is assigned seven linguistic fuzzy subsets varying from negative big (NB) to positive big (PB). Each subset is associated with a triangular membership function to form a set of seven membership functions for each fuzzy variable.

The variables are normalized by multiplying with respective gains K_{in1} , K_{in2} , K_{out} so that their value lies between -1 and 1. The membership functions of the input output variables have 50% overlap between adjacent fuzzy subsets. The membership function for acceleration, speed and voltage are shown in Fig. 1.7

NB	NEGATIVE BIG
NM	NEGATIVE MEDIUM
NS	NEGATIVE SMALL
ZE	ZERO
PS	POSITIVE SMALL
PM	POSITIVE MEDIUM
PB	POSITIVE BIG

Table 1: Membership functions for fuzzy variables

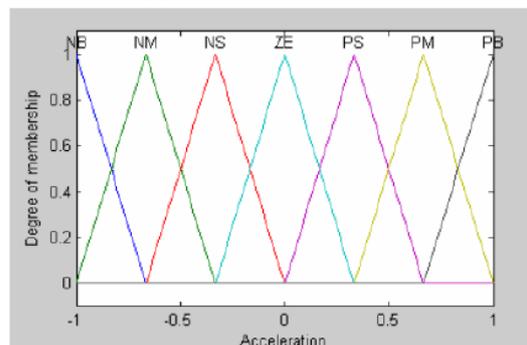


Fig. 1.7(a) Membership functions for acceleration

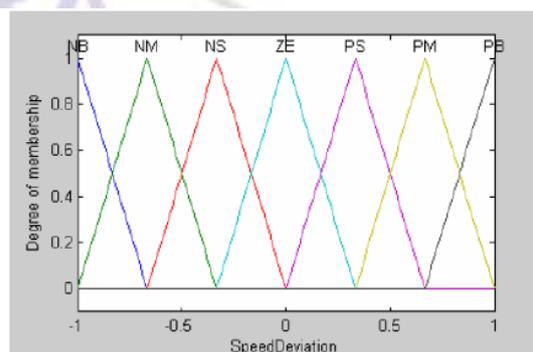


Fig. 1.7(b) Membership functions for speed deviation

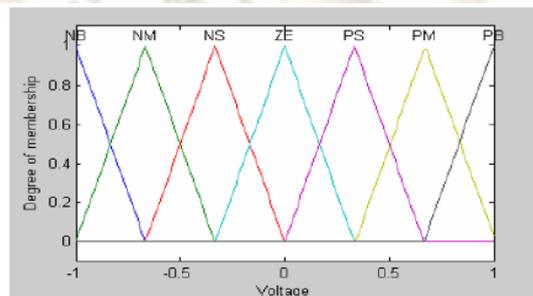


Fig. 1.7(c) Membership functions for voltage

iii. FUZZY RULE BASE

A set of rules which define the relation between the input and output of fuzzy controller can be found using the available knowledge in the area of designing PSS. These rules are defined using the linguistic variables. The two inputs, speed and acceleration, result in 49 rules for each machine. The typical rules are having the following structure:

Rule 1: If speed deviation is NM (negative medium) AND acceleration is PS (positive small) then voltage (output of fuzzy PSS) is NS (negative small).

Rule 2: If speed deviation is NB (negative big) AND acceleration is NB (negative big) then voltage (output of fuzzy PSS) is NB (negative big).

Rule 3: If speed deviation is PS (positive small) AND acceleration is PS (positive small) then voltage (output of fuzzy PSS) is PS (positive small) and so on....

All the 49 rules governing the mechanism are explained in Table 2 where all the symbols are defined in the basic fuzzy logic terminology.

Speed Deviation	Acceleration						
	NB	NM	NS	ZE	PS	PM	PB
NB	NB	NB	NB	NB	NM	NM	NS
NM	NB	NM	NM	NM	NS	NS	ZE
NS	NM	NM	NS	NS	ZE	ZE	PS
ZE	NM	NS	NS	ZE	PS	PS	PM
PS	NS	ZE	ZE	PS	PS	PM	PM
PM	ZE	PS	PS	PM	PM	PM	PB
PB	PS	PM	PM	PB	PB	PB	PB

Table 2: Rule base of fuzzy logic controller

IV. DEFUZZIFICATION

The input for the defuzzification process is a fuzzy set (the aggregate output fuzzy set) and the output is a single crisp number. As much as fuzziness helps the rule evaluation during the intermediate steps, the final desired output for each variable is generally a single number. However, the aggregate of a fuzzy set encompasses a range of output values, and so must be defuzzified in order to resolve a single output value from the set. The most popular defuzzification method is the centroid calculation, which returns the center of area under the curve and therefore is considered for defuzzification. For a discretised output universe of discourse

$$Y = (y_1, \dots, y_p)$$

Which gives the discrete fuzzy centroid, the output of the controller is given by following expression:

$$u_k = \frac{\sum_{i=1}^p y_i w_i}{\sum_{i=1}^p w_i}$$

V. SIMULATION MODEL AND RESULT

The performance of single machine infinite bus system has been studied without excitation system, with excitation system only, with conventional PSS (lead-lag) and with fuzzy logic based PSS. The dynamic models of synchronous machine, excitation system and conventional PSS are described. The machine data is taken from

TABLE I

Parametres	Numerical values
P	0.9
Q	0.3
E _t	1.0
F	50
X _d	1.81
X _q	1.76
X _{d1}	0.3
X _L	0
X _e	0.65
R _a	0.003
T _{do1}	8.0
H	3.5
Ω _o	314
K _D	0
T _R	0.02
E _{Tmag}	1.0
L _{adu}	1.65
L _{adu}	1.60
R _{fd}	.0006
L _{fd}	0.153
K _{sd}	0.8491
K _{sq}	0.8491
K _{sd1}	0.434
K _{sq1}	0.434
A _{SAT}	0.031
B _{SAT}	6.93
ψ ₁	0.8
Frequency of oscillation (in rad/sec)	10

i. Performance with constant field voltage-

The model used in the simulink to study the response of the system with constant field voltage is shown in figure. In this representation the dynamic characteristics are represented in terms of K constant. The values of K constants are calculated using above parameters are- K1=0.7636, K2=0.8644, K3=0.3231, K4=1.4189

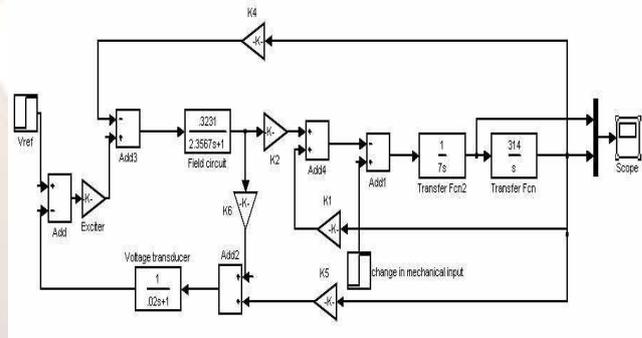


Fig 1.8: Simulink model for simulation of single machine infinite bus System with constant field voltage.

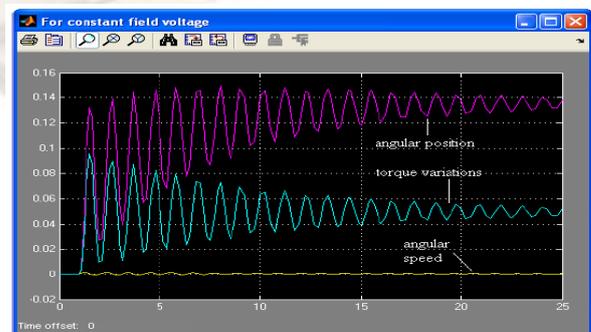


Fig 1.9: System response for a 5% change in mechanical input

iv. Performance with Fuzzy Logic Based PSS-

The Model used in Simulink/Matlab to analyze the effect of fuzzy logic controller in damping small signal oscillations when implemented on single machine infinite bus system is shown below in Fig.1.17 and the details of the fuzzy controller are shown in Fig. 1.16. As shown in Fig. 1.17, the fuzzy logic controller block consists of fuzzy logic Block and scaling factors. The input scaling factors are two, one for each input and one scaling factor for output which determine the extent to which controlling effect is produced by the controller. The performance of fuzzy logic controller is studied for the scaling factors having the values as $K_{in1}=1.6$, $K_{in2}=29.56$, $K_{out}=1.06$.

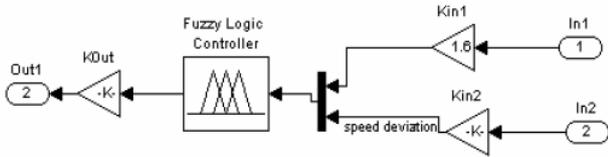


Fig 1.16: Fuzzy logic based PSS

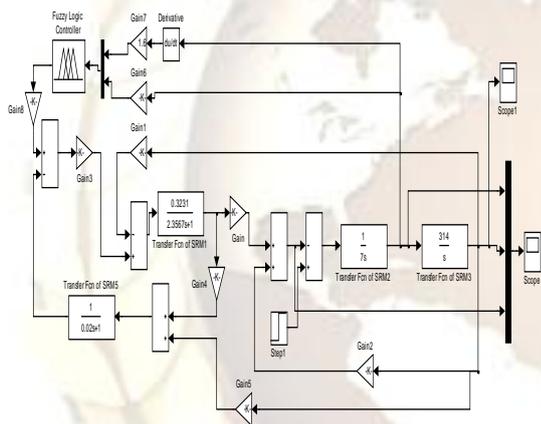


Fig 1.17: Simulink model with fuzzy logic based PSS

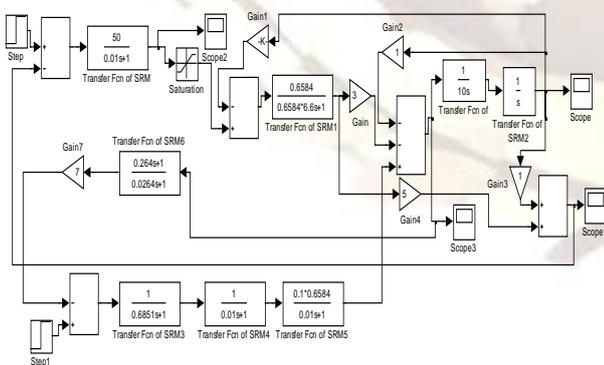


Fig 1.18: Mode of PSS

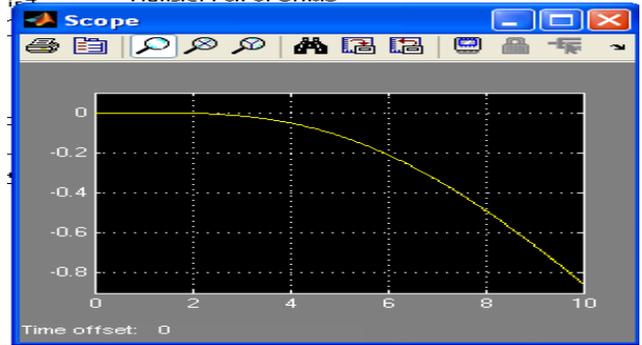


Fig. 1.19 output Result of Scope

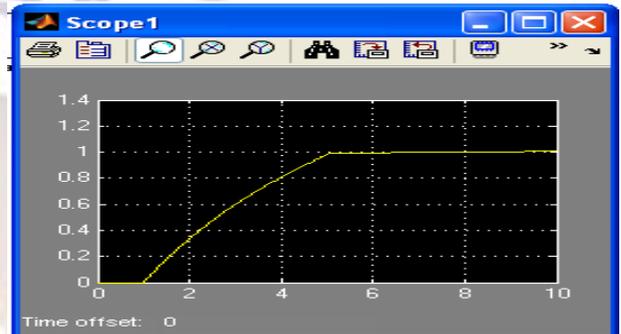


Fig. 1.20 Result of Scope 1

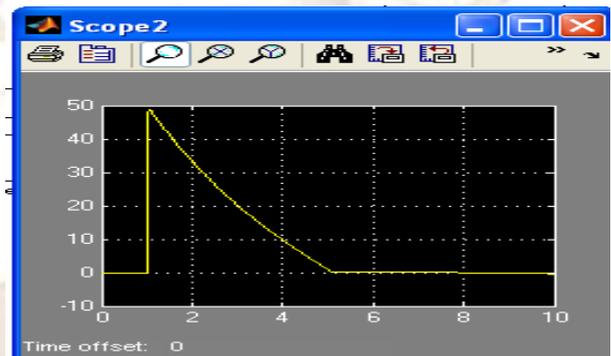


Fig. 1.21 output Result of Scope2

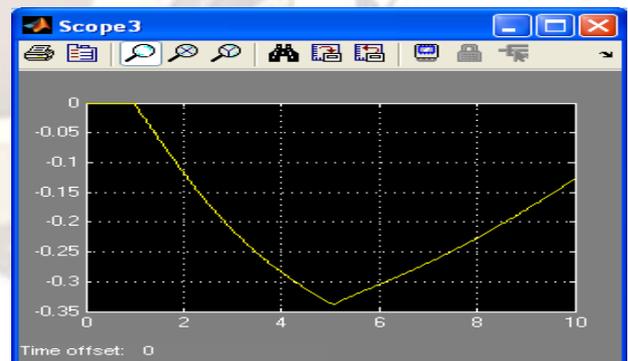


Fig. 1.22 output Result of Scope

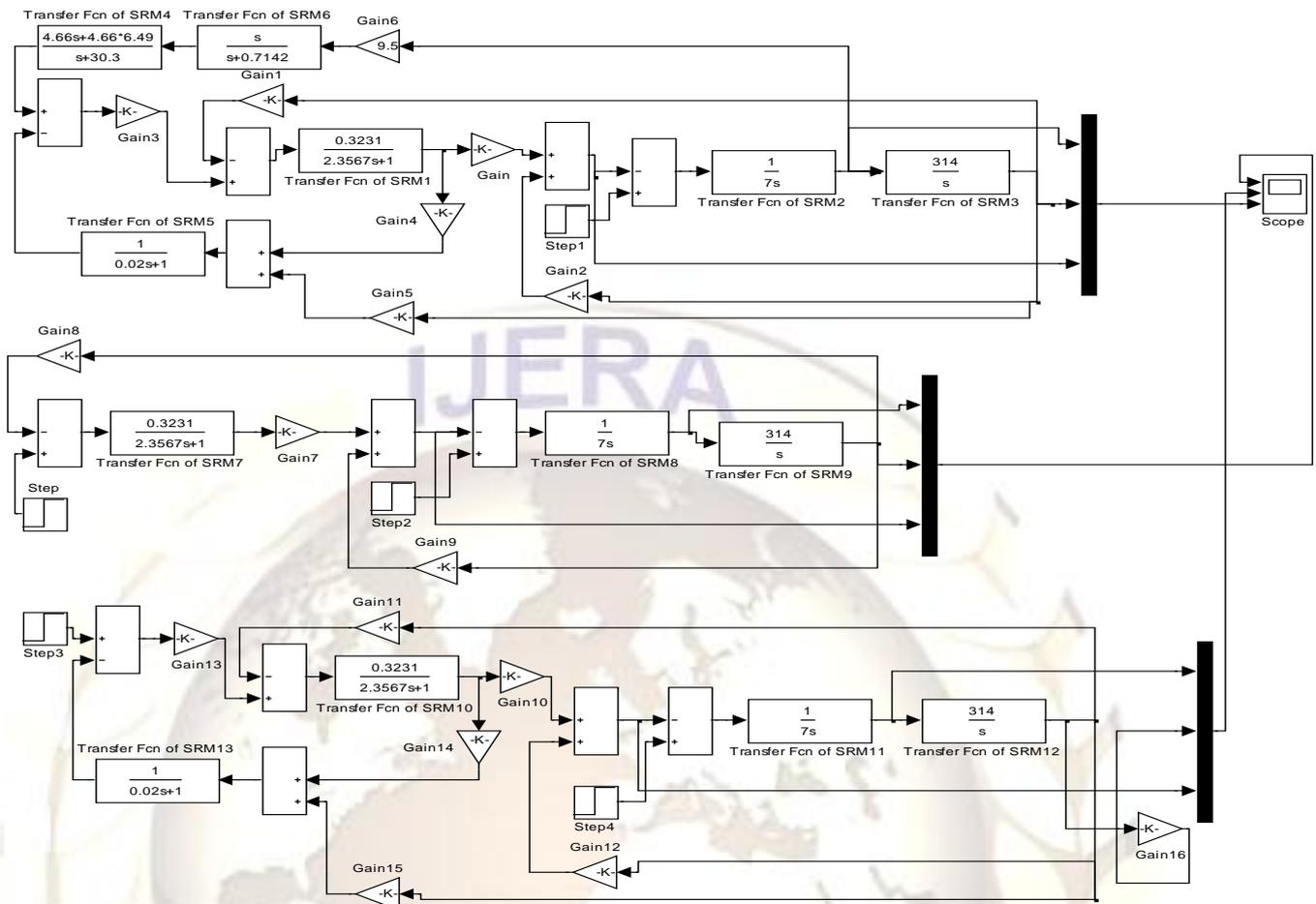


Fig. 1.23 Simulation Model of AVR with PSS

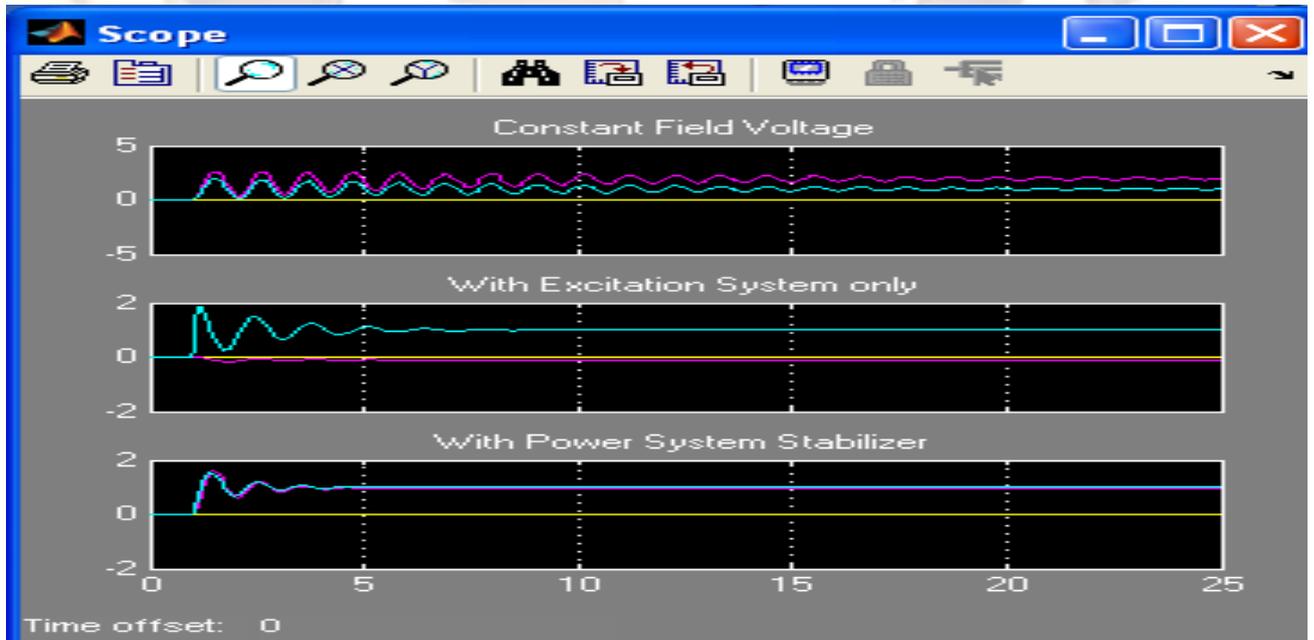


Fig. 1.24 Simulation Result of AVR with PSS

VI. FUZZY INFERENCE SYSTEM

Fuzzy logic block is prepared using FIS file in Matlab 7.5 and the basic structure of this file is as shown in Fig 1.25. This is implemented using following FIS (fuzzy Inference System) properties:

And Method: Min
Or Method: Max
Implication: Min
Aggregation: Max
Defuzzification: Centroid

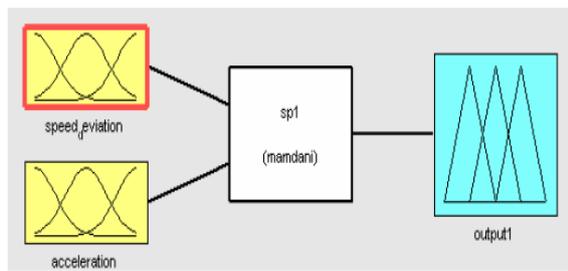


Fig 1.25 Fuzzy Inference Systems

For the above FIS system Mamdani type of rule-base model is used. This produces output in fuzzified form. Normal system need to produce precise output which uses a defuzzification process to convert the inferred possibility distribution of an output variable to a representative precise value. In the given fuzzy inference system this work is done using centroid defuzzification principle. In this min implication together with the max aggregation operator is used.

Given FIS is having seven input member function for both input variables leading to 7×7 i.e. 49 rules.

VII. COMPARISON OF RESULTS

To compare the performance of lead-lag PSS and fuzzy logic based PSS, the step response are shown in Fig. 1.26 and Fig. 1.27 for angular speed for the negative and the positive values of K5.

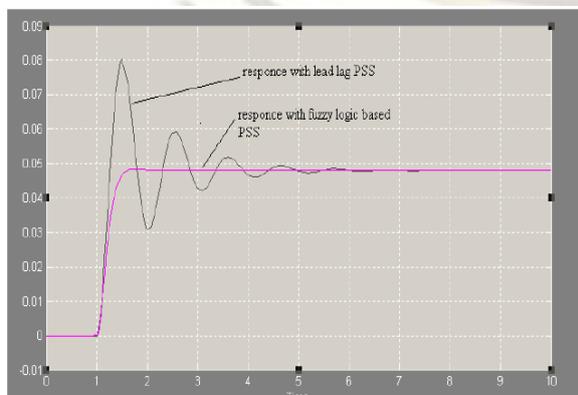


Fig 1.26: Comparison of angular position for a 5% change in mechanical input with conventional PSS

(lead-lag) and fuzzy logic based PSS with K5 negative.

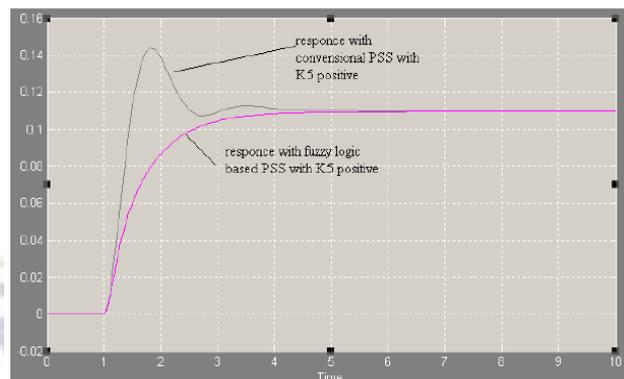


Fig 1.27: Comparison of angular position for a 5% change in mechanical input with conventional PSS (lead-lag) and fuzzy logic based PSS with K5 positive

These results are for 5% change in mechanical torque. From Fig. 1.26 and Fig. 1.27 it can be perceived that with the application of fuzzy logic the rise time and the settling time of the system decreases. The system reaches its steady state value much earlier with fuzzy logic power system stabilizer compared to conventional power system stabilizer for negative K5. For the positive value of K5, the sluggish response (over damped response) characteristic is resulted and the settling time remains largely unchanged.

The step response characteristics for angular position for both lead-lag PSS and fuzzy logic based PSS are compared in Fig. 1.28 and Fig. 1.29 for negative and positive values of K5.

From relative plots it can be retrieved that oscillations in angular speed reduces much faster with fuzzy logic power system stabilizer than with conventional power system stabilizer for both the cases i.e. when K5 positive and negative. As shown in Fig. 1.29 with fuzzy logic the variation in angular speed reduces to zero in about 2seconds but with conventional power system stabilizer it takes about 6 seconds to reach to final steady state value and also the oscillations are less pronounced in fuzzy logic based PSS. Similar is the case with K5 positive.

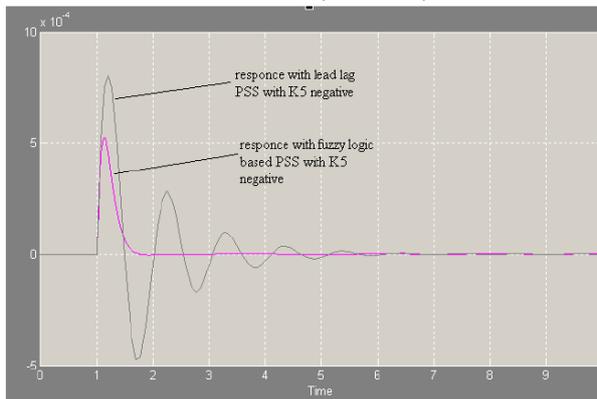


Fig 1.28: Comparison of angular speed for a 5% change in mechanical input with conventional PSS (lead-lag) and fuzzy logic based PSS with K5 negative.

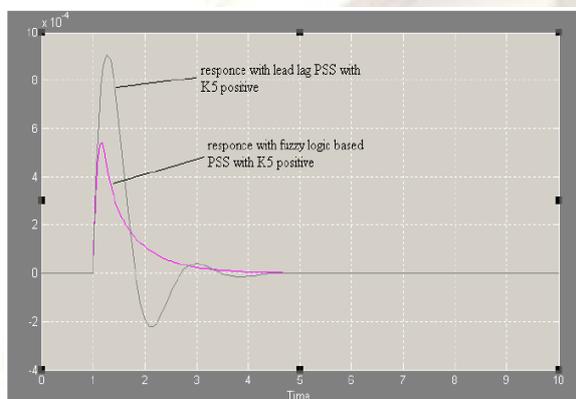


Fig 1.29: Comparison of angular speed for a 5% change in mechanical input with conventional PSS (lead-lag) and fuzzy logic based PSS with K5 positive.

Therefore, it can be inferred that the fuzzy controller does not require any complex mathematical support and the response is much improved than with conventional PSS.

VIII. CONCLUSION

The target of the developed work is the damping of oscillations related to power system using a controller based on fuzzy logic theory on a single machine to infinite bus system. The proposed controller provides a more robust control over a large excursion of the operating points versus an optimal controller and lead-lag stabilizer. The conventional lead-lag PSS is not giving desired performance under wide range of operating conditions. A methodology to site the proposed controller doesn't depend on the Eigen value analysis approach. In this thesis work initially the effectiveness of power system stabilizer in damping power system stabilizer is reviewed then fuzzy logic power system stabilizer is introduced after taking speed deviation and acceleration of synchronous generator as the input signals to the fuzzy controllers and voltage as the output signal.

FPSS shows the better control performance than power system stabilizer in terms of settling time and damping effect. The proposed FPSS produces better damping effect than PSS. It is thus possible to realize the controller efficiently. The over damped response is resulted with positive K5, which is normally not encountered in practical situations. Therefore, it can be concluded that the performance of the proposed FPSS is much better and the oscillations are damped out much quicker.

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